Ground-Water and Surface-Water Hydrology of Camp Swift, Bastrop County, Texas

Final Report

R. Stephen Fisher, Principal Investigator
Robert E. Mace
Erika Boghici

assisted by Conrad A. Kuharic and Martina Blüm

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Adjutant General's Department of Texas

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James F. Resner II

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T. James Fries, Project Manager

Bureau of Economic Geology Noel Tyler, Director The University of Texas at Austin Austin, Texas 78713-8924

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CONTENTS

| EXECUTIVE SUMMARY | 1 |
|--|----|
| INTRODUCTION | 2 |
| Regional Setting | 2 |
| Geology and Hydrostratigraphy | 4 |
| METHODS | 8 |
| Ground-Water Analysis | 8 |
| Well Inventory | |
| Monitor Well Installation | 9 |
| Well Testing | 10 |
| Ground-Water Sampling | 10 |
| Surface-Water Analysis | 11 |
| Watershed Delineation | 11 |
| Floodplain Analysis | 11 |
| Surface-Water Quality | 13 |
| GIS Data Preparation | 13 |
| GROUND-WATER HYDROLOGY | 14 |
| Well Inventory | 14 |
| Monitoring Well Construction | 19 |
| Ground-Water Levels | 19 |
| Hydraulic Properties | 21 |
| Ground-Water Chemistry | 25 |
| Conceptual Flow Model | |
| SURFACE-WATER HYDROLOGY | 39 |
| Principal Streams and Watersheds | 39 |
| Stream-flow Duration and Flood Frequency | 39 |
| Floodplain Analysis | 39 |
| GIS DATA PREPARATION | 43 |
| SUMMARY | 43 |
| ACKNOWLEDGMENTS | 44 |
| REFERENCES | 44 |
| APPENDICES | |
| Well survey around the camp perimeter | 49 |
| 2. Detailed well schematics and drilling reports for monitor wells | 55 |
| 3. Water-level and water-quality data from Powell Bend Mine | 61 |
| Data dictionary for GIS coverages | 69 |

Figures

| 1. | Index map showing location of Camp Swift, major highways and towns, and ecological provinces | 3 |
|-----|---|------|
| 2. | Generalized geologic map, schematic cross section, and stratigraphic column, Bastrop and easternmost Travis Counties | 5 |
| 3. | Geologic map of Camp Swift | 6 |
| 4. | Well locations on Camp Swift including monitor wells drilled during this study | . 15 |
| 5. | Private wells located near Camp Swift | . 18 |
| 6. | Water levels measured in the alluvium and the Hooper, Simsboro, and Calvert Bluff Formations in Bastrop County | . 20 |
| 7. | Water levels measured in the Simsboro Formation at the Powell Bend Lignite Mine in Bastrop County | . 22 |
| 8. | Water-level map of the shallow Calvert Bluff and Simsboro Formations in the Camp Swift area | . 24 |
| 9. | Histograms of specific capacity for the Calvert Bluff, Simsboro, and Hooper Formations in Bastrop County | |
| 10. | Results of a bail test at SWIFT-1 | . 27 |
| 11. | Results of a bail test at SWIFT-2 | . 28 |
| 12. | Histograms showing total dissolved solids for the alluvium, the Calvert Bluff Formation, the Simsboro Formation, and the Hooper Formation in Bastrop County | . 33 |
| 13. | Trilinear diagrams showing ground-water chemical composition for the alluvium and the Calvert Bluff Formation in Bastrop County | |
| 14. | Trilinear diagrams showing ground-water chemical composition for the Simsboro and Hooper Formations in Bastrop County | . 36 |
| 15. | Schematic of the conceptual ground-water flow model for Camp Swift | |
| 16. | Watershed delineations for Camp Swift | . 40 |
| 17. | Mean daily flow, flow duration, and flood frequency analysis for Big Sandy Creek near Camp Swift | |
| 18. | One-hundred-year floodplains for Camp Swift | . 42 |
| | | |
| | Tables | |
| 1., | Water-level measurements in Camp Swift wells | . 23 |
| 2. | Most recent chemical analyses of ground water from the alluvium, Calvert Bluff Formation, Simsboro Formation, and Hooper Formation | |
| 3. | Chemical analyses of ground water from Camp Swift monitor wells | . 37 |

EXECUTIVE SUMMARY

Ground-water and surface-water investigations of Camp Swift, Bastrop County, Texas, were conducted to provide the Texas Army National Guard with information needed to preserve environmental quality and resources while planning and conducting training and preparedness activities. Spatial information such as surface geology, watersheds, elevation data, floodplains, well locations, and water levels was converted to digital files and submitted to the Texas Army National Guard Geographic Information System office at Camp Mabry, Austin, Texas, for future use in managing the training facility. Similar investigations were conducted on Camps Barkeley, Bowie, Mabry, and Maxey, and Fort Wolters. Results of those studies are presented separately.

Previously published reports and public data files were examined to obtain background information on the camp and surrounding area. These data were used to guide more focused studies on the training facility. Ground-water studies included locating existing wells on and near the camp; installing new wells as needed; testing and sampling selected wells; determining ground-water levels, chemical compositions, and aquifer hydraulic properties; and developing a conceptual model of ground-water flow. Surface-water studies focused on delineating watersheds and mapping floodplains.

The principal ground-water sources at Camp Swift are strata in the Wilcox Group. From deepest to shallowest, these units are the Hooper, Simsboro, and Calvert Bluff Formations and alluvium along Big Sandy and McLaughlin Creeks and Dogwood Branch. Wells in the Hooper and Simsboro Formations show a gradual recovery from low levels during the drought years in the 1950's. Wells in the Calvert Bluff and alluvium show fluctuating but generally steady water levels over the same time period. Water levels in the Calvert Bluff are higher than those in the Simsboro, indicating potential for downward ground-water flow. Such flow is probably slow because low-permeability strata separate the two aquifer units. Ground waters are fresh to brackish, changing with depth from a calcium-bicarbonate type in alluvium to mixed calcium-bicarbonate and sodium-chloride types in the Hooper Formation.

Camp Swift resides in the Colorado River Basin drainage area. Most of the camp grounds are within the Dogwood Creek, McLaughlin Creek, or Dogwood Branch subdrainage basins. Areas that would be flooded after a 100-yr storm are confined to the immediate vicinity of Dogwood Branch. Flooded areas are larger in the McLaughlin Creek subdrainage basin, and they are widest in the northeastern portion of the training facility.

INTRODUCTION

This report summarizes ground-water and surface-water studies at Camp Swift, Bastrop County, Texas, conducted by the Bureau of Economic Geology (BEG) for the Texas Army National Guard. This work was part of a larger study of Texas Army National Guard training facilities that included Camp Barkeley (Taylor County), Camp Bowie (Brown County), Camp Mabry (Travis County), Camp Maxey (Lamar County), and Fort Wolters (Parker County). These investigations, in conjunction with aquatic and biological surveys conducted by the Texas Parks and Wildlife Department, provide information needed by the Texas Army National Guard to plan training and preparedness activities in a way that will protect and enhance environmental resources without compromising training needs and national security readiness. Reports of similar investigations on the other training facilities are presented separately.

This report contains results of hydrogeologic and hydrologic analyses and describes how we prepared data files for Geographic Information System (GIS) coverages of the camp and surrounding area. The hydrogeologic analyses contain information regarding hydrostratigraphy, camp and perimeter well surveys, monitor well drilling, well testing, aquifer properties, groundwater levels, ground-water chemistry, and a conceptual ground-water flow model. The hydrologic analyses contain information regarding streams and drainage basins on and near the camp, watershed delineations, stream-flow duration, flood frequency, and floodplain analysis. The GIS data preparation section contains descriptions of the original data sets, how they were obtained, and how they were processed to obtain GIS coverages for the camp.

Regional Setting

Camp Swift is located in Bastrop County between the cities of Bastrop and Elgin on the upper Gulf Coastal Plain (fig. 1). The area is characterized by nearly level to gently sloping ridge tops with generally steep side slopes and narrow to broad valleys. Drainage channels are clearly incised in valleys and are part of the Colorado River Basin drainage area (Baker, 1979).

Soils on the camp consist of the Patilo-Demona-Silstid and the Axtell-Tabor associations (Baker, 1979). The Patilo-Demona-Silstid association has gently sloping ridge tops to strongly sloping side slopes. The Patilo and Demona soils have a sandy surface layer and slightly to moderately permeable lower layers on the uplands, usually consisting of sandy clay or sandy clay loam. Silstid soils are mostly confined to drainage areas and foot slopes. The Axtell-Tabor association has nearly level to gently sloping ridge tops and gently to strongly sloping side slopes.

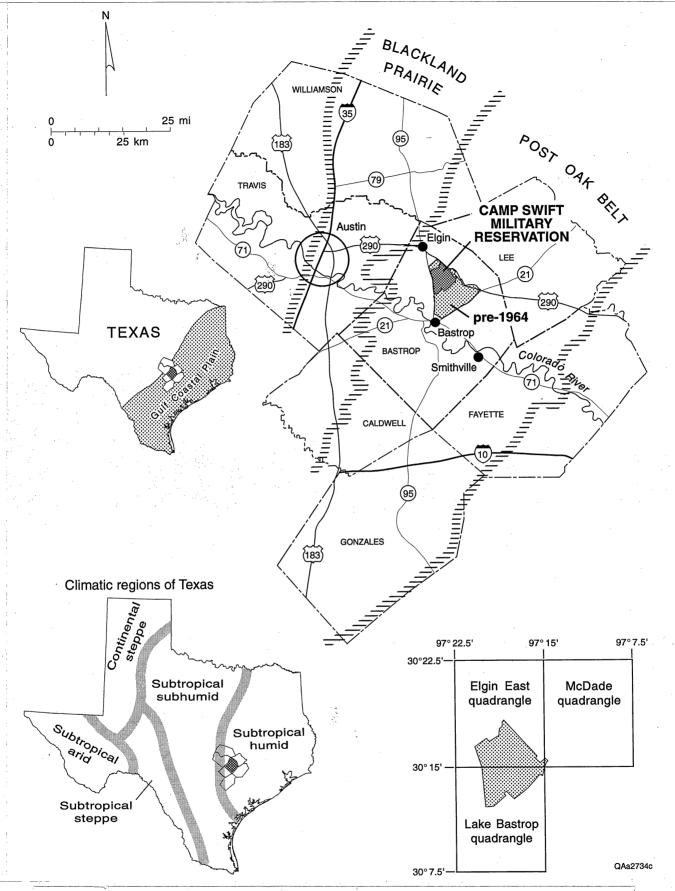


Figure 1. Index map of Central Texas region showing location of Camp Swift study area (darkly shaded area), major highways and towns, and immediate ecological provinces (Blackland Prairie and Post Oak Belt); lightly shaded area around Camp Swift indicates extent of base before transfer to Texas Army National Guard in 1964. Insets show climatic regions of Texas (after Larkin and Bomar, 1983) and 7.5-minute topographic quadrangles containing study area (from Avakian and Wermund, 1993).

These soils have a loamy surface layer and very slightly permeable lower layers, usually consisting of mottled clay or sandy clay.

Camp Swift lies within in the Oak-Hickory vegetation region (Kier and others, 1977) delineated westward by the Blackland Prairie and eastward by the Fayette Prairie (Tharp, 1939). In Bastrop County the Blackland Prairie and Oak-Hickory zones merge, with timber groves standing as islands in the prairie vegetation and as grassland inclusions in the oak-hickory forest (Tharp, 1939). In addition to the native woods and grasslands, there are croplands, cleared pastures, and rangelands (Baker, 1979).

Camp Swift is located in the subtropical humid climate region (fig. 1) (Larkin and Bomar, 1983). The climate is dominated by tropical marine air from the Gulf of Mexico, modified by a westward decrease in moisture content. The influence of continental air varies seasonally (Larkin and Bomar, 1983).

The closest recording weather station is in Austin, Texas, about 22 miles west of Camp Swift. Reports from the Austin station show that winds are typically from the south and southeast throughout the year. Average wind speeds range from 8 to 11 mph, with highest speeds in April and lowest speeds in July and October (Bomar, 1983). On average about 21 cold fronts per year move through Austin, usually accompanied by northerly winds (Bomar, 1983).

The mean annual precipitation measured in Austin is 31.5 inches, with highest precipitation rates between May and October (Bomar, 1983). Mean monthly low temperatures range from 39°F in January to 74°F in July, averaging 58°F. Mean monthly high temperatures range from 59°F during the coldest month of winter to a high of 95°F in July, with an average of 79°F.

The average annual gross lake-surface evaporation rate ranges from 59 inches in the eastern part of Bastrop County to 61 inches toward the west. Highest rates of approximately 8 inches occur during July, and lowest rates of about 2.5 inches occur during January (Larkin and Bomar, 1983).

Geology and Hydrostratigraphy

The Calvert Bluff Formation and creek alluvium underlie Camp Swift (figs. 2 and 3). The Calvert Bluff Formation is the upper formation of the Wilcox Group, which also includes the Hooper Formation (lower) and the Simsboro Formation (middle) (fig. 2). The Calvert Bluff Formation consists of weakly to moderately consolidated, massive to thin-bedded, clayey, finegrained to very fine grained sandstone, siltstone, and claystone (Avakian and Wermund, 1993).

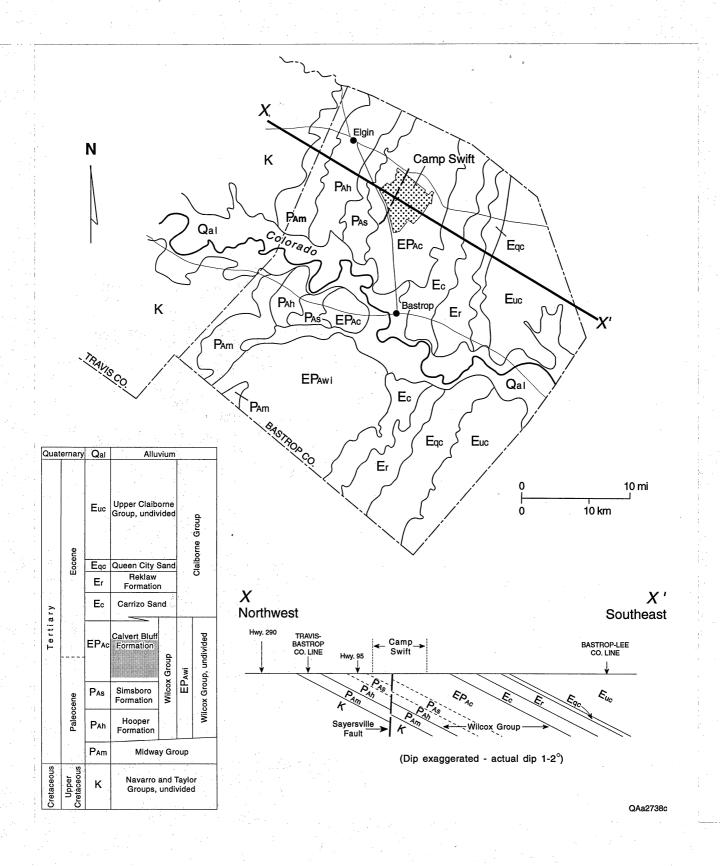


Figure 2. Generalized geologic map, schematic cross section, and stratigraphic column for Bastrop and easternmost Travis Counties (from Avakian and Wermund, 1993).

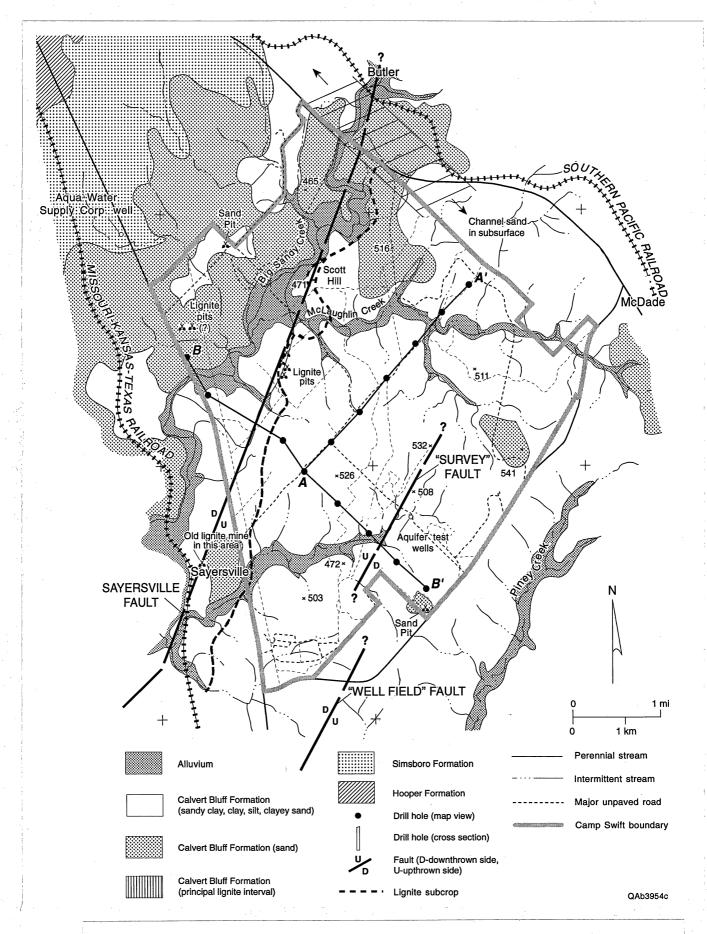


Figure 3. (a) Geologic map of Camp Swift (adapted from Avakian and Wermund, 1993).

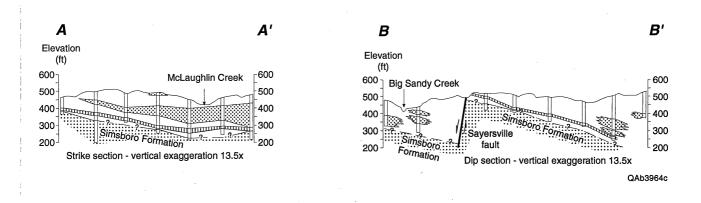


Figure 3. (b) Geologic cross sections of Camp Swift (adapted from Avakian and Wermund, 1993).

The formation varies from light gray in sandy units to brown in muddy units and typically weathers yellowish-brown to red. Lignite beds and ironstone concretions are common in the lower 200 ft and occur less commonly higher in the formation. Beneath Camp Swift, the thickness of the Calvert Bluff Formation ranges from as little as 25 ft near the Sayersville Fault to as much as 500 ft beneath the southwestern edge of Camp Swift (Gaylord and others, 1985) (figs. 2 and 3). The Calvert Bluff Formation is sandier in the northern reaches and in a few small areas in the southern part of the camp (Henry and Basciano, 1979) (fig. 3).

Unconsolidated alluvium and colluvium underlie stream valleys and form thin veneers on upland surfaces north of Sandy Creek (fig. 3) (Avakian and Wermund, 1993). Principal locations of alluvium are along Big Sandy Creek, McLaughlin Creek, and Dogwood Branch (fig. 3). Stream-valley alluvium consists of interbedded clay, silt, and sand with varying amounts of gravel. The veneers on the upland surfaces are part of the soil profile and contain abundant pebbles and cobbles of petrified wood, quartzite, and other siliceous rocks.

Follett (1970) recognized the Wilcox Group as the most important water-bearing strata in Bastrop County. The Simsboro and Hooper Formations are the main water-producing intervals in the Wilcox Group, both of which underlie Camp Swift (fig. 2). The Simsboro Formation consists mostly of weakly to slightly consolidated, crossbedded kaolinitic quartz sandstone with some siltstone and claystone (Avakian and Wermund, 1993). The Hooper Formation consists of mudstone, sand, and sandstone with a few thin and discontinuous beds of lignite (Avakian and Wermund, 1993).

METHODS

Ground-Water Analysis

The Camp Swift area has been previously characterized by investigations of lignite resources and mining potential as well as hydrogeologic and physical environment studies. Reports by the Texas Water Development Board (TWDB) (Austin, 1954; Follett, 1970; Thorkildsen and Price, 1991), U.S. Geological Survey (USGS) (Guyton, 1942; Gaylord and others, 1985), The University of Texas at Austin Bureau of Economic Geology (BEG) (Avakian and Wermund, 1993), U.S. Department of Interior (1982), and Argonne National Laboratory (Dennis, 1993) summarize much of the general hydrogeologic information for the area. Other more specific hydrogeology reports were prepared by Hydro-Search, Inc. (1981), and Science Applications, Inc. (1982). Geologic information related to lignite resources was included in BEG

reports by Kaiser and others (1978), Henry and Basciano (1979), Henry and others (1980), and Kaiser and others (1980). These reports and data listings provided a regional hydrogeologic framework and guided our site-specific studies to those areas of the camp where hydrogeologic information was sparse.

Our methods of investigation included a well inventory on and off the camp, installation of monitor wells, well testing, and ground-water sampling. We used all this information to develop a conceptual model, or general idea, of how ground water flows in the Camp Swift area.

Well Inventory

We conducted inventories on the camp and around the perimeter of the camp to locate and, if possible, measure wells. On the camp, we tried to locate all wells. This was accomplished through interviews with National Guard archeologists and camp personnel. In addition, we drove on all camp roads in our search for wells. Old topographic maps (circa 1904) provided guidance for locating potential wells near old homesteads on the camp. For all located wells, we made detailed measurements and descriptions of well location, type, depth, water level, diameter, and casing construction.

The perimeter well survey was required because mapping water levels and understanding ground-water systems at the training facility required data beyond the site boundaries and because the data base available from State agencies typically contained records for less than half of the existing wells in an area. The perimeter well survey also provided information concerning the use of local ground-water resources in proximity to the camp and potential receptors to ground-water flowing beneath the camp. Our approach to the perimeter well survey was to search for wells visible from the roadway, meet the well owners, and measure water levels and electrical conductivities in as many wells as possible. In addition, we interviewed residents and local drillers regarding ground-water wells and general ground-water conditions.

Monitor Well Installation

Monitor wells were installed to obtain hydrogeologic data from poorly characterized areas on the camp. The installation of monitor wells at Camp Swift included selecting and staking appropriate sites for well locations, arranging access to the well sites and a water source, drilling and purging the borehole, installing casing, and developing the cased well.

We drilled the monitor wells with a Central Mine Equipment 75 drilling rig. Depending on the geology, we used hollow stem augering, solid stem boring, rotary/wet coring, or a combination thereof to install the wells. Where possible, we collected core and cuttings for inspection. After the well was drilled, we augered or flushed the cuttings from the hole and developed the well with a bailer, usually removing one to two wellbore volumes of water. Well completion consisted of installing 2-inch well screen and pipe, placing a sandpack around the screen, placing a bentonite seal above the sandpack, grouting to within a few feet of land surface, installing a well guard, and cementing the guard in place with a well pad. We installed either 10- or 20-ft-long 0.010-inch slotted screen in the wells. The sandpack consisted of 20/40 sand and straddled the screen. We installed locking above-ground well guards on each of the wells. Once the well was completed and the cement had dried, we developed the well again with a bailer or an electrical submersible pump.

Well Testing

We conducted bail tests in the two wells we drilled on the camp. We also attempted to test a hand-dug well and a USGS well. The bail tests involved using a bailer to quickly remove water from the well and monitoring water-level recovery with an electronic water-level meter. Recovery data were input into a spreadsheet, and transmissivity was interpreted using the Hvorslev (1951) method and the Cooper and others (1967) curve matching method. A hand-dug well in the northern part of the camp was tested, but we found that the water level never recovered because the well was probably sealed from the aquifer. The USGS well had its wellbore blocked by debris.

Ground-Water Sampling

Ground-water samples were collected from the two monitoring wells drilled during this project. In both cases, samples were obtained by bailing the well. Our procedure was to first remove and discard one bailer volume (~500 mL) to rinse the bailer before sampling. A second bailer volume was then collected and used to measure pH and temperature at the well site. Water from the next bailer run was used to rinse field filtration equipment. Ground water produced by subsequent bailer runs was passed through a 0.45 µm filter and collected in sample bottles that had first been rinsed three times with filtered sample water. Aliquots intended for cation and trace metal analyses were preserved by adding 5 mL of 6N nitric acid to each 500 mL sample to lower the pH to a value less than 2. Aliquots for all other analyses were filtered but otherwise untreated.

Surface-Water Analysis

Several surface-water studies have previously been conducted in the Camp Swift area. Gaylord and others (1985) monitored four stream-flow gauges in the immediate area and analyzed flood hydrographs for Big Sandy Creek and Dogwood Creek. Peak discharges for these creeks were determined by U.S. Bureau of Land Management (U.S. Department of the Interior, 1980). FEMA (1991) estimated 100-yr floodplains for the Camp Swift area. Avakian and Wermund (1993) prepared drainage basin maps for the camp area.

Watershed Delineation

Maps delineating watersheds on training facilities are important tools for combining training activities with environmental stewardship. Providing watershed delineations based on digital elevation data in GIS format rather than as paper copy has the advantages that (1) map coverages can be exported to the Texas National Guard for their use in other applications and (2) such digital data can subsequently be developed into watershed models in which the effects of various scenarios of precipitation amount and duration can be examined. Digital elevation models (DEMs) at the 1:24,000 scale are currently available for the Elgin, Lake Bastrop, and McDade quadrangles, which include the Camp Swift area. For this report, we generated watershed maps from the DEM data using routines provided in the ArcInfo (ESRI, 1993) software package.

Floodplain Analysis

We further constrained FEMA (1991) floodplain maps by conducting a more detailed analysis of smaller tributaries in the watersheds. Floodplain analysis involves determining the area adjacent to a river or stream that will flood for a specified return period (for example, a 100-yr flood). The standard procedure is to determine the 100-yr flood at key points on the stream and use backwater computation to determine stages upstream (Linsley and others, 1982, p. 452). If available, the 100-yr flood is statistically determined from the stream-gauge record. In the case of Camp Swift, long-term discharge data are available on Big Sandy Creek on the outlet side of the camp. In cases where these data are lacking, regional frequency methods or loss rate and unit hydrograph techniques applied to the 100-yr rainfall data can be used (Linsley and others, 1982, p. 452).

Our floodplain analysis consisted of (1) designing 100-yr 24-h synthetic storms, (2) determining the 100-yr flood hydrographs at strategic points in the watersheds,

(3) determining 100-yr flooding surfaces, and (4) mapping the 100-yr floodplains on 1:24,000 USGS topographic maps.

To design the 100-yr 24-h synthetic storms, we first used maps published by the U.S. Weather Bureau (Herschfield, 1961, as shown in Chow, 1964, p. 9–56) to determine the 100-yr 24-h rainfall. We then used these rainfall rates with the SCS Type II distribution (Bedient and Huber, 1988) to generate the storms.

To determine the 100-yr flood hydrographs, we used HEC-1 (Hydrologic Engineering Center, 1981) with SCS unit hydrographs (Soil Conservation Service, 1957) and Muskingum routing (McCarthy, 1938). Input to HEC-1 included subbasin drainage area, runoff curve numbers, basin lag, routing storage coefficient, and routing weight factor. Runoff curve numbers are used to define the unit hydrographs and are a function of soil type, vegetation, land use, antecedent moisture, and the hydrologic properties of the catchment surface. Basin lag, also called catchment lag, is the elapsed time, or response time, between rainfall and runoff occurrence and is partly a function of hydraulic length, catchment gradient, drainage density, and drainage patterns. The routing storage coefficient, or time constant, is a function of the channel reach length and the speed of the flood wave. The routing weight factor is a function of the flow and channel characteristics that affect the dispersion of the flood wave downstream.

We delineated detailed subwatersheds and determined subwatershed drainage area with ArcInfo (ESRI, 1993). We calculated weighted curve numbers in ArcInfo for each subwatershed using STATSGO (Soil Conservation Service, 1991) digital hydrologic soil data and land-use data assuming moderate antecedent moisture conditions ($I_a = 0.25$ inch). Because the majority of the watersheds were not gauged, we estimated the basin lag, t_p , using (Linsley and others, 1982, p. 224):

$$t_p = C_t \left(\frac{LL_c}{\sqrt{s}}\right)^n \tag{1}$$

where C_t is a constant that varies between 1.8 and 2.2 for units of miles (Snyder, 1938), L is the stream distance to the divide, L_c is the stream distance, n is 0.35 for valley drainage areas (Linsley and others, 1982, p. 225), and s is the channel gradient. For this study, we chose a mean C_t value of 2.0. We assigned the routing storage coefficient to 0.20, a typical value for most natural streams (Linsley and others, 1982, p. 219). We measured L, L_c , and s from USGS 1:24,000 topographic sheets. We estimated the routing traveltime constant, K, using (Linsley and others, 1982, p. 465–541):

$$K = \frac{bL\sqrt{A}}{\sqrt{s}} \tag{2}$$

where A is the drainage area and b is a constant between 0.04 and 0.08 for b in miles and b in square miles. For this study, we chose a mean b value of 0.06. With the above data input into HEC-1, we modeled 100-yr flood hydrographs for subwatersheds on or just outside the camp. We recorded peak flows for these 100-yr flood hydrographs for assessing flooding depths.

We used HEC-RAS (Hydrologic Engineering Center, 1995) to estimate 100-yr flooding surfaces at the locations where we determined the flood hydrographs. Input to HEC-RAS included: topographic cross sections at hydrograph locations, stream lengths between cross sections, Manning's *n* values, discharge rates, and stream-flow boundary conditions. We measured topographic cross sections from USGS 1:24,000 topographic sheets perpendicular to the stream path. Using a map roll gauge, we measured stream lengths between cross sections from the topographic sheets. We assumed Manning's *n* values to be 0.06 on the banks (Hydrologic Engineering Center, 1995) and 0.05 in and near the stream channel. HEC-1 supplied the peak 100-yr discharge rates for each hydrograph location. We assigned the stream-flow boundary condition at the output end of the model as a critical depth boundary. In all simulations, we assumed subcritical flow. After inputting the above information, HEC-RAS determined the flood surface at each of the chosen locations.

We mapped the 100-yr floodplains by transcribing the 100-yr flood surfaces estimated by HEC-RAS onto USGS 1:24,000 topographic sheets and interpolated between hydrograph locations. Once mapped, we digitized the floodplains in ArcInfo GIS and printed maps.

Surface-Water Quality

Water-quality data is available for many of the stream-flow gauging stations near training facilities. The information was obtained in digital form from the USGS.

GIS Data Preparation

Wherever possible, spatial information was input to a geographic information system (GIS). Data bases with spatial coordinates were uploaded into the GIS, and interpreted data such as contour maps were digitized and attributed. The information was imported to the ArcInfo GIS software system so data coverages could be overlaid and compared with each other. Well

postings and hydrologic and hydrogeologic analyses were posted on new USGS topographic maps to facilitate data transfer and to ensure the best possible spatial accuracy.

A data dictionary was prepared for the coverages so that subsequent users can know the methods of data preparation and the accuracy of the information. GIS data files were delivered to the Adjutant General's Office of the Texas Army National Guard at Camp Mabry for inclusion in their GIS program.

GROUND-WATER HYDROLOGY

Well Inventory

Archeological reports; TWDB records; conversations with Sergeant West, Camp Swift Facility Manager; and a field survey of camp grounds provided information for locating wells on Camp Swift. We located seven wells or well sites and identified eight other potential sites that may have wells but that we could not locate during our survey of Camp Swift (fig. 4).

- CSW-B001 is a 4-inch-diameter drilled well with a measured depth greater than 200 ft and a water level of 109 ft below land surface. The casing is made of PVC and extends 1.00 ft above grade. The well is located within a small fenced area and does not have a locking well vault. Well and water depths are difficult to measure because the wellbore is very crooked. The USGS drilled this well to assess the local geology and measure selected hydrogeologic properties of the Wilcox Group as related to potential lignite mining on Camp Swift (Gaylord and others, 1985). At completion, this well (USGS #C-12, TWDB #58-54-303) was 220 ft deep and completed in the basal part of the Calvert Bluff Formation with screen from 200 to 220 ft.
- CSW-B002 is a 4-inch-diameter drilled well with a measured depth of 72 ft and a water level 66.2 ft below land surface. The casing is made of PVC and extends 0.5 ft above grade. The well is located within a small fenced area 50 ft south of CSW-B001 and does not have a locking well vault. The USGS drilled this well to assess the local geology and measure selected hydrogeologic properties of the Wilcox Group as related to potential lignite mining on Camp Swift (Gaylord and others, 1985). At completion, this well (USGS #C-13, TWDB #58-54-304) was 330 ft deep and completed in the upper part of the Simsboro Formation with screen from 250 to 330 ft. Our depth measurement of 75 ft suggests that either this well has caved or there is an obstruction in the well.

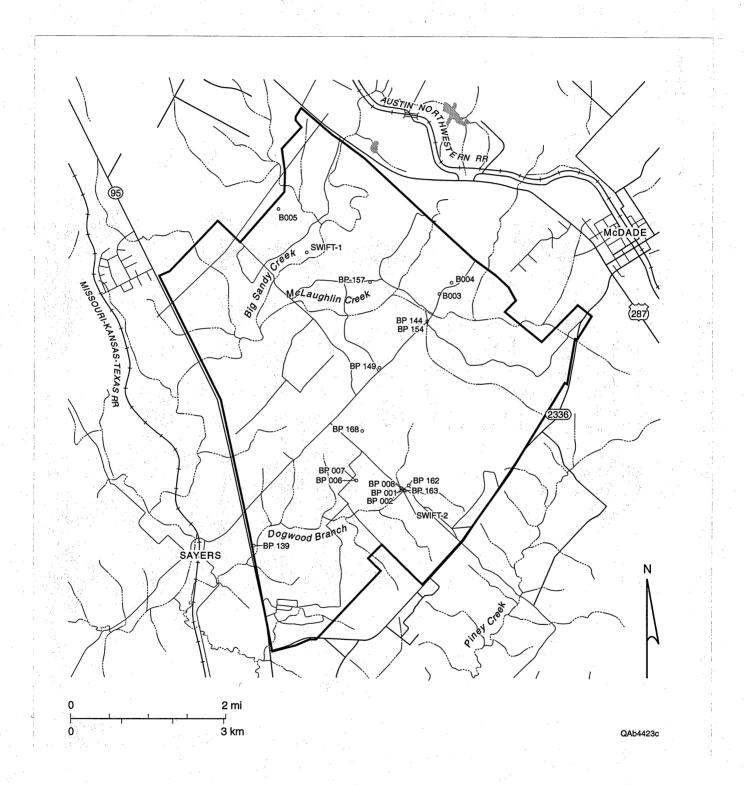


Figure 4. Well locations on Camp Swift including monitor wells drilled during this study.

- CSW-B003 is a hand-dug cistern located at an old home site. The cistern has a diameter of 3 ft with a brick crown that extends 0.43 ft above ground surface. The cistern is 16.4 ft deep and currently holds no water. Cistern sides appear to be sealed with mortar. The cistern is uncovered and holds several pieces of trash. This cistern is noted by the cultural resources staff of the Adjutant General's Department as the 41BP156 site or Westbrook Housesite (William R. Furr, personal communication, 1995).
- CSW-B004 is a hand-dug cistern located at an old home site several feet from CSW-B003. The cistern has a diameter of 3 ft with a brick crown that extends 1 ft above ground surface. The cistern is 15.4 ft deep and currently holds no water. Cistern sides appear to be sealed with mortar. The cistern is uncovered and contains several pieces of trash. This cistern is noted by the cultural resources staff of the Adjutant General's Department as the 41BP156 site or Westbrook Housesite (William R. Furr, personal communication, 1995).
- **CSW-B005** is a hand-dug well located near the northern boundary of the camp. The well has a diameter of 2.5 ft with a brick crown that extends 3.5 ft above ground surface. The well is 18.5 ft deep with a depth to water of 13.5 ft. The sides of the well are made of brick at least to water level and probably to depth. The cistern is uncovered and contains some debris. There was an oily sheen on the water surface when we surveyed this well.
- CSW-B006 is a cistern in the southwest part of the camp. The cistern has a diameter of 3 ft and does not protrude above ground surface. The cistern is filled with debris to 3 ft below ground surface, uncovered, and holds no water. This cistern is noted by the cultural resources staff of the Adjutant General's Department as the 41BP158 site or Beck Housesite (William R. Furr, personal communication, 1995).
- CSW-B007 is a partially filled cistern 20 ft east of CSW-B006. The cistern has a diameter of 3 ft and does not extend above ground level. The cistern is filled with debris to 8 ft below ground surface, is uncovered, and holds no water. This cistern is noted by the cultural resources staff of the Adjutant General's Department as the 41BP158 site or Beck Housesite (William R. Furr, personal communication, 1995).
- CSW-B008 is a 4-inch-diameter drilled well of unknown depth and a water level of 77 ft below land surface. The casing is made of PVC and extends 1.5 ft above grade. The well is located within a small fenced area 50 ft north of CSW-B001 and does not have a

locking well vault. The USGS drilled this well to assess the local geology and measure selected hydrogeologic properties of the Wilcox Group as related to potential lignite mining on Camp Swift (Gaylord and others, 1985). At completion, this well (USGS #C-11, TWDB #58-54-302) was 500 ft deep and completed in the Simsboro Formation with screen from 240 to 490 ft.

The cultural resources staff of the Adjutant General's Department report several other locations as possible well sites (William R. Furr, personal communication, 1995). However, we were unable to locate wells or cisterns at any of these sites. At a few sites we found what appeared to be mounds of dirt in the approximate location of the well sites. Therefore, many of these wells may have been filled since the archeological survey. There may be other historic wells on Camp Swift yet to be discovered. These wells will be difficult to locate because of the thick brush and changing anthropogenic landmarks.

During the 1970's, more than 70 lignite exploration wells were drilled on Camp Swift. These boreholes have apparently been backfilled, and no record of their existence is filed with the TWDB or the Texas Natural Resources Conservation Commission. Gaylord and others (1985) include a map showing the locations of these boreholes.

A total of 83 wells were mapped during the well survey around the camp perimeter (fig. 5) (app. 1). Measurements of water level and/or conductivity data were obtained from 15 wells. Well depths given for 31 wells ranged from 40 to 1,100 ft for private wells and from 505 to 1,558 ft for municipal water-supply wells. Of the 31 wells, 12 were 100 ft deep or less, 8 ranged from 101 to 250 ft deep, 9 ranged from 400 to 750 ft deep, and 2 were more than 1,000 ft deep. Depth to water, measured in nine wells and estimated by the owners for four others, ranged from 20 to 50 ft in seven wells, from 51 to 60 ft in two wells, and from 61 to 100 ft in one well; it was greater than 150 ft in three wells. In addition, one well of 80-ft depth was flowing, and one of 50- to 60-ft estimated depth was dry. Measured electrical conductance values ranged from 480 to 725 $\mu\Omega$, or approximately 300 to 465 mg/L total dissolved solids (TDS). These data show that all measured wells had fresh water (<1000 mg/L TDS). High iron content was a common observation of well users. In general, well water is used for domestic purposes, including yard and garden irrigation. The presence of at least two water-supply systems in the general area appears to be reducing reliance on private wells as a source of domestic water.

One local driller informed us that water-producing sands are insufficiently continuous to make generalizations about well depths in any given area. Wells in the area appear to produce from the Wilcox Group; most wells are probably producing from the Simsboro Formation, with the

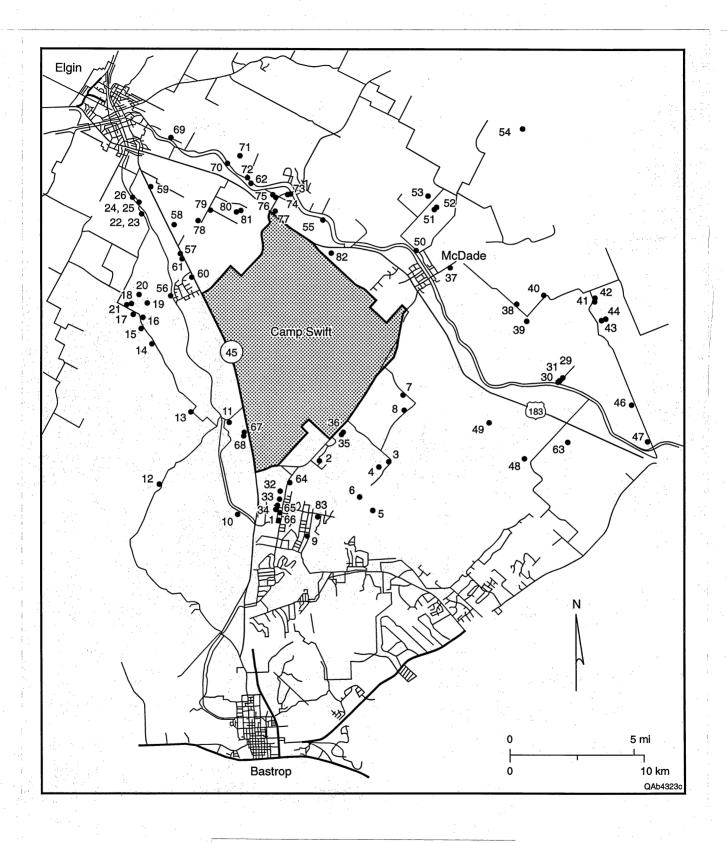


Figure 5. Private wells located near Camp Swift.

possible exception of some shallow, hand-dug wells in the Calvert Bluff Formation and the two deep wells (>1000 ft), which may produce from the Hooper Formation.

Monitoring Well Construction

We drilled and completed two wells in the Calvert Bluff Formation on Camp Swift. Well SWIFT-1 is located in the northern part of the camp (fig. 4) and is 57.1 ft deep in the sandy portion of the Calvert Bluff Formation. Well SWIFT-2 is located in the central part of the camp near the USGS well field (fig. 4) and is 51 ft deep in the clayey portion of the Calvert Bluff Formation. We used solid stem boring to install SWIFT-1 and hollow stem augering to install SWIFT-2. Detailed well schematics and drilling reports are included in appendix 2.

Ground-Water Levels

TWDB board files had sufficient water-level data to construct long-term hydrographs for the Hooper Formation (fig. 6a), the Simsboro Formation (fig. 6b), the Calvert Bluff Formation (fig. 6c), and the alluvium (fig. 6d). A well (58-46-102) drilled into the Hooper Formation 1 mi north of Elgin shows an increase in water level after a period of steady levels during the 1950's (fig. 6a). This well is located in the outcrop of the Hooper Formation and is likely showing water-level recovery since the major drought during the 1950's. Ground-water pumpage has not caused large local or regional declines in Bastrop County (Follett, 1970).

A well (58-46-301) drilled into the Simsboro Formation 5 mi east of Elgin shows a similar water-level response (fig. 6b) to the well in the Hooper Formation (fig. 6a). This Simsboro well is located in the outcrop and again is likely showing water-level recovery since the major drought during the 1950's.

A well (58-61-201) drilled into the Calvert Bluff Formation outcrop 5 mi west of Bastrop shows a rather steady water-level elevation with small fluctuations likely due to variations in rainfall (fig. 6c). A well (58-60-301) drilled into Cedar Creek alluvium overlying the Wilcox Group outcrop about 10 mi west of Bastrop also shows a relatively steady water-level elevation with small fluctuations likely due to variations in rainfall (fig. 6d).

We also obtained water-level data from monitor wells at the Powell Bend lignite mine from the Railroad Commission of Texas (RRC). The Powell Bend lignite mine is located to the southwest of Camp Swift and has five wells that have been measured over the last 9 yr. These wells were drilled through the Calvert Bluff Formation and into the upper Simsboro Formation

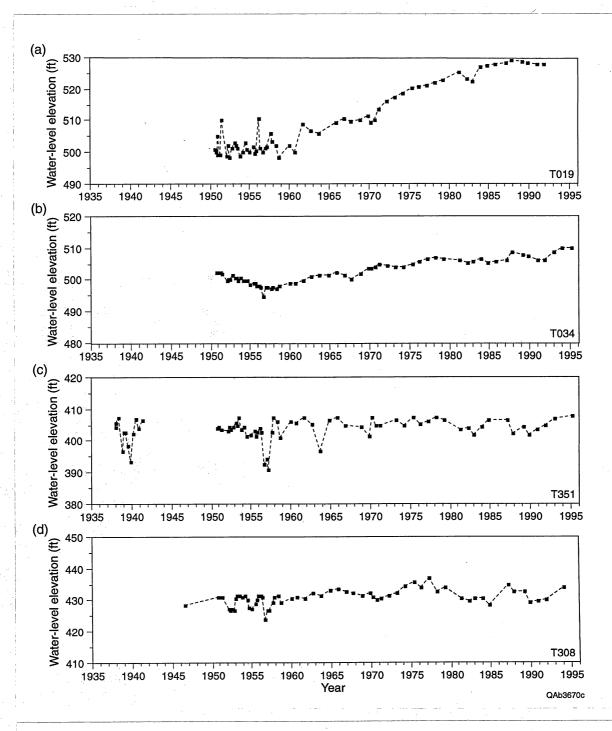


Figure 6. Water levels measured in Bastrop County in (a) the Hooper Formation in well 58-46-102, (b) the Simsboro Formation in well 58-46-301, (c) the Calvert Bluff Formation in well 58-61-201 and (d) alluvium overlying the Wilcox Group in well 58-60-301.

where they were completed. The purpose of the wells was to monitor water-level and water-chemistry fluctuations to assess impact of surface mining of lignite. The wells show somewhat similar water-level responses, with a period of little water-level change from 1987 to mid-1992 and water-level oscillations since mid-1992 (fig. 7). Other hydrographs from formations in the Bastrop and Camp Swift area are included in Avakian and Wermund (1993), Follett (1970), and Thorkildsen and Price (1991).

Water levels in wells on the camp did not show much variation during the course of the project (table 1). There is a decline in water level in well SWIFT-1 from November 1995 to March 1996 that is perhaps due to seasonal variation (there was very little rainfall during this time). Well CSW-B001 (in the Simsboro) had water levels drop 1.2 ft from August to November, 1995. Water levels in the other camp wells were fairly steady.

Measurements in the USGS wells show that the water-level elevation in the Calvert Bluff Formation is about 40 ft higher than the water-level elevation in the underlying Simsboro Formation. This indicates that there is a downwardly directed ground-water flow gradient that will cause ground water from the Calvert Bluff to move downward into the Simsboro. This vertical transfer of ground water probably occurs at a slow rate owing to low-permeability beds between the two aquifers.

Water levels in the Calvert Bluff are strongly influenced by topography, with water flow generally directed downslope. Figure 8 shows our interpretation of water levels in the Calvert Bluff in the Camp Swift area. Our interpretation differs from Gaylord and others (1985) because we used our two shallow wells to constrain mapping inside the camp, whereas Gaylord and others did not have any water-level information inside the camp in the shallow Calvert Bluff. Water level in SWIFT-1 was deeper than we would have expected given the anticipated topographic control on water levels. This anomaly might be due to the close proximity of the well (~2,000 ft) from the Sayersville Fault (fig. 2), which has over 200 ft of throw. It is possible that the fault plane acts to redirect Calvert Bluff ground water into the Simsboro Formation.

Water levels in the Simsboro Formation are moving downdip in a generally uniform manner with cones of depression near large municipal well fields (fig. 9).

Hydraulic Properties

Various aquifer tests have been performed in each of the formations either reported in TWDB files or in publications. Alluvium in Bastrop County has two measured well yields of 25 and

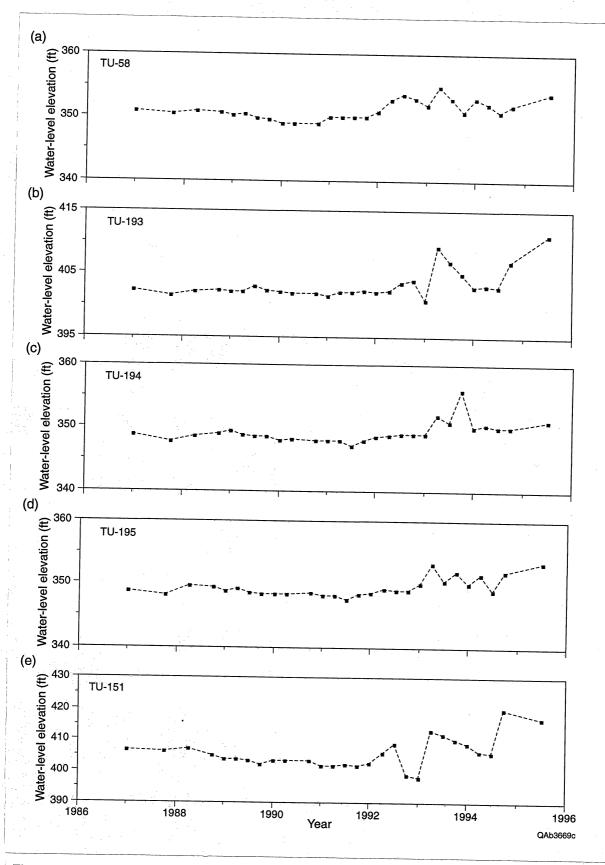


Figure 7. Water-level fluctuations in the Simsboro Formation underlying the Calvert Bluff Formation at the Powell Bend lignite mine just southwest of Camp Swift. Note that TU-151 (e) is at a different scale.

Table 1. Water-level measurements in Camp Swift wells.

| Date Time Depth to water (ft) Water-lever elevation (ft) SWIFT-1 11/2/95 0932 37.99 414.01 11/21/95 1035 39.34 412.66 3/6/96 0927 39.78 412.22 SWIFT-2 3/6/96 1050 38.69 433.86 CSW-B001 9/25/95 1100 108.85 361.15 11/21/95 1147 110.09 359.91 3/6/96 1120 110.10 359.90 CSW-B002 9/25/95 1115 66.81 403.19 11/21/95 1147 66.94 403.06 3/6/96 3/6/96 1120 66.86 403.14 CSW-B005 9/26/95 0955 17 453 11/21/95 1100 17.78 452.22 3/6/96 1010 17.61 452.39 CSW-B008 9/25/95 77 393 11/21/95 1147 78.67 391.33 3/6/96 1120 | | | | |
|---|--------------------------------|--------------|----------------|------------------|
| 11/2/95 0932 37.99 414.01 11/21/95 1035 39.34 412.66 3/6/96 0927 39.78 412.22 SWIFT-2 3/6/96 1050 38.69 433.86 CSW-B001 9/25/95 1100 108.85 361.15 11/21/95 1147 110.09 359.91 3/6/96 1120 110.10 359.90 CSW-B002 9/25/95 1115 66.81 403.19 11/21/95 1147 66.94 403.06 3/6/96 1120 66.86 403.14 CSW-B005 9/26/95 0955 17 453 11/2/95 0944 17.65 452.35 11/21/95 1100 17.78 452.22 3/6/96 1010 17.61 452.39 CSW-B008 9/25/95 - 77 393 11/21/95 1147 78.67 391.33 | Date | Time | water | |
| 3/6/96 1050 38.69 433.86 CSW-B001 9/25/95 1100 108.85 361.15 11/21/95 1147 110.09 359.91 3/6/96 1120 110.10 359.90 CSW-B002 9/25/95 1115 66.81 403.19 11/21/95 1147 66.94 403.06 3/6/96 1120 66.86 403.14 CSW-B005 9/26/95 0955 17 453 11/2/95 0944 17.65 452.35 11/21/95 1100 17.78 452.22 3/6/96 1010 17.61 452.39 CSW-B008 9/25/95 - 77 393 11/21/95 1147 78.67 391.33 | 11/2/95 11/21/95 | 1035 | 39.34 | 412.66 |
| 9/25/95 1100 108.85 361.15 11/21/95 1147 110.09 359.91 3/6/96 1120 110.10 359.90 CSW-B002 9/25/95 1115 66.81 403.19 11/21/95 1147 66.94 403.06 3/6/96 1120 66.86 403.14 CSW-B005 9/26/95 0955 17 453 11/2/95 0944 17.65 452.35 11/21/95 1100 17.78 452.22 3/6/96 1010 17.61 452.39 CSW-B008 9/25/95 - 77 393 11/21/95 1147 78.67 391.33 | | 1050 | 38.69 | 433.86 |
| 9/25/95 1115 66.81 403.19 11/21/95 1147 66.94 403.06 3/6/96 1120 66.86 403.14 CSW-B005 9/26/95 0955 17 453 11/2/95 0944 17.65 452.35 11/21/95 1100 17.78 452.22 3/6/96 1010 17.61 452.39 CSW-B008 9/25/95 - 77 393 11/21/95 1147 78.67 391.33 | 9/25/95 11/21/95 | 1147 | 110.09 | 359.91 |
| 9/26/95 0955 17 453 11/2/95 0944 17.65 452.35 11/21/95 1100 17.78 452.22 3/6/96 1010 17.61 452.39 CSW-B008 9/25/95 - 77 393 11/21/95 1147 78.67 391.33 | 9/25/95 11/21/95 | 1147 | 66.94 | 403.06 |
| 9/25/95 - 77 393 11/21/95 1147 78.67 391.33 | 9/26/95 11/2/95 11/21/95 | 0944 1100 | 17.65 17.78 | 452.35 452.22 |
| | 9/25/95 11/21/95 | | 78.67 | 391.33 |

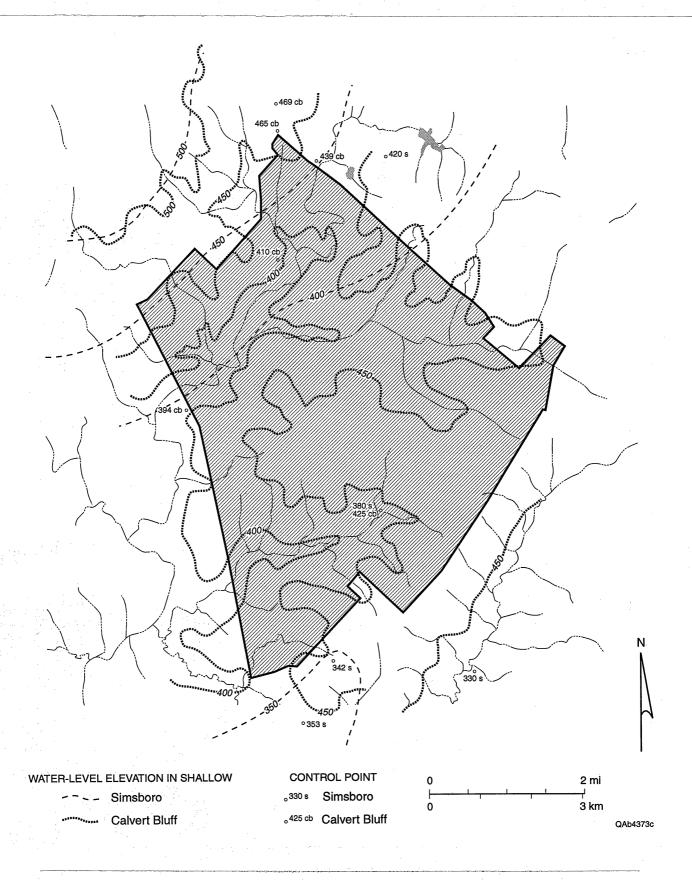


Figure 8. Water-level map of the shallow Calvert Bluff and Simsboro Formations in the Camp Swift area

75 gal/min. The Calvert Bluff Formation has well yields that range from 3 to 600 gal/min with a geometric mean of 80 gal/min and specific capacities that range from 38 to 800 ft² d⁻¹ with a geometric mean of 251 ft² d⁻¹ (fig. 10a). Using the method of Razack and Huntley (1991), this mean specific capacity corresponds to a transmissivity of 1,400 ft² d⁻¹. We did not find any pumping test reports for wells in the Calvert Bluff Formation in the area.

The Simsboro Formation has well yields that range from 11 to 1,200 gal/min with a geometric mean of 250 gal/min and specific capacities that range from 630 to 10,000 ft² d⁻¹ with a geometric mean of 2,500 ft² d⁻¹ (fig. 10b). Using the method of Razack and Huntley (1991), this mean specific capacity corresponds to a transmissivity of 4,300 ft² d⁻¹. The average values of transmissivity and storativity of the old Camp Swift wells tested by Guyton (1942) are 6,000 ft² d⁻¹ and 0.0004, respectively (Gaylord and others, 1985).

The Hooper Formation has well yields that range from 8 to 250 gal/min with a geometric mean of 80 gal/min and specific capacities that range from 77 to 520 ft² d⁻¹ with a geometric mean of 250 ft² d⁻¹ (fig. 10c). Using the method of Razack and Huntley (1991), this mean specific capacity corresponds to a transmissivity of 1,400 ft² d⁻¹.

We conducted site-specific aquifer tests in the monitor wells we drilled in the Calvert Bluff on Camp Swift. Monitor well SWIFT-1, drilled into the sandy portion of the Calvert Bluff, had a transmissivity of about 9 to 10 ft² d⁻¹ based on the interpretation of a bail test (fig. 11). Monitor well SWIFT-2, drilled into the clayey portion of the Calvert Bluff, had a transmissivity of about 0.7 ft² d⁻¹ based on the interpretation of a bail test (fig. 12).

Ground-Water Chemistry

TWDB files contain water chemistry data for the alluvium and the Calvert Bluff, Simsboro, and Hooper Formations for Bastrop County (table 2). TDS for the alluvium range from 291 to 612 mg/L with a geometric mean of 380 mg/L (fig. 13a). TDS for the Calvert Bluff Formation range from 226 to 2,187 mg/L with a geometric mean of 500 mg/L (fig. 13b). Three of the samples (12 percent) were brackish (1,000 mg/L < TDS < 10,000 mg/L). TDS for the Simsboro Formation range from 129 to 1,116 mg/L with a geometric mean of 380 mg/L (fig. 13c). Two of the samples (5 percent) were brackish. TDS for the Hooper Formation range from 246 to 1,411 mg/L with a geometric mean of 490 mg/L (fig. 13d). Two of the samples (13 percent) were brackish.

Waters from the alluvium are calcium-bicarbonate in composition (fig. 14a). Waters from the Calvert Bluff Formation are sodium-bicarbonate and calcium-sulfate in composition (fig. 14b).

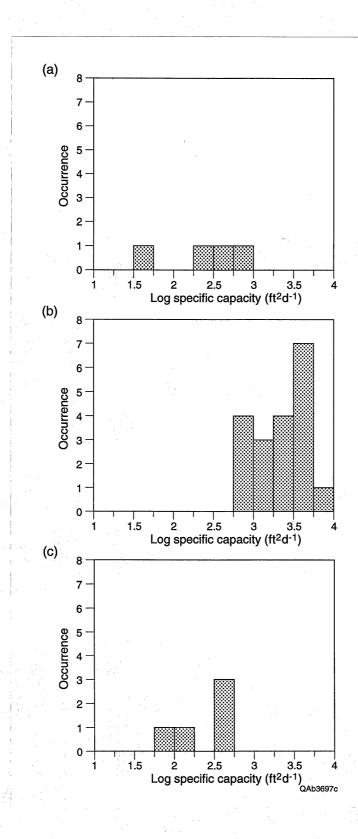


Figure 9. Histograms of specific capacity for the (a) Calvert Bluff, (b) Simsboro, and (c) Hooper Formations in Bastrop County.

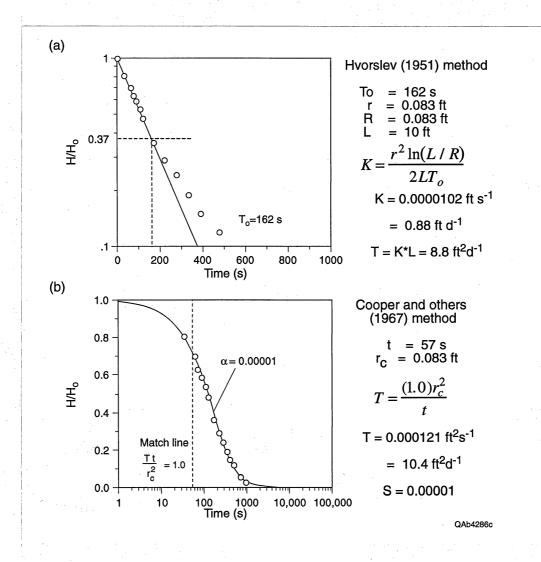


Figure 10. Results of a bail test at SWIFT-1.

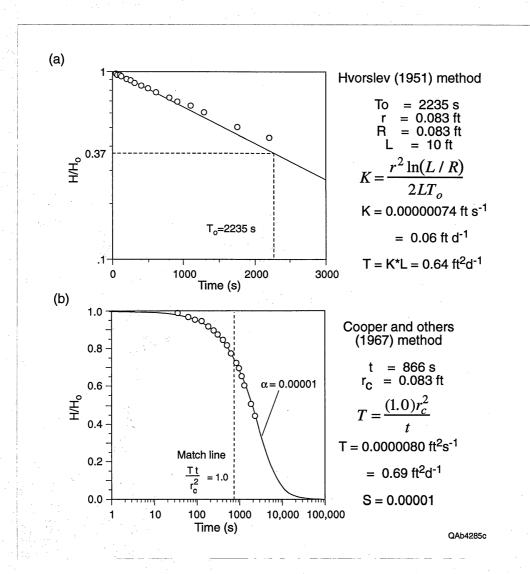


Figure 11. Results of a bail test at SWIFT-2.

Table 2. Most recent chemical analyses of ground waters from the alluvium, Calvert Bluff Formation, Simsboro Formation, and Hooper Formation.

| Spec. cond. (mΩ) | | 905 | 268 | . 1 | 630 | 549 | 572 | 755 | 597 | 700 | | 260 | 462 | 1 | 1090 | 366 | 790 | 1 | 1420 | 1040 | 268 | . 1 | 006 | 449 | 370 | 4134 | 584 | 1340 | 474 | 481 | 592 | 487 |
|--|-----------|---------|----------|--------|---------|---------|------------|------|----------|---------|--------------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|------------|---------|
| Total ardness mg/L) | | 449 | 270 | 203 | • | 224 | 1 | 326 | 253 | 332 | | 161 | 88 | 1680 | ı | 83 | 292 | 806 | 534 | 440 | 221 | 1000 | 270 | 83 | 86 | 1606 | 210 | 590 | 158 | 199 | 129 | 96 |
| Total Total alk hardness (mg/L) (mg/L) | | 382 | 244.26 | 222.13 | 269.67 | 203.28 | 196.72 | 234 | 237.7 | 293 | | 74 | 147.54 | | 40.15 | 6.56 | 182 | 204.92 | 150.82 | 198.36 | 136.07 | 298.36 | 0 | 177.05 | 37.7 | 427 | 121.31 | 221.31 | 100 | 164 | 189 | 183.61 |
| TDS (mg/L) | | 612 | 346 | 357 | 383 | 291 | 295 | 478 | 357 | 377 | | 319 | 273 | 1 | ı | 307 | 489 | 1688 | 943 | 728 | 365 | 1375 | 573 | 279 | 226 | 2187 | 347 | 968 | 278 | 335 | 331 | 300 |
| hЧ | | 7.4 | 8.2 | 7.3 | 7.4 | 7.4 | 7.3 | 7.2 | 7.6 | 7.5 | | 6.7 | 8.3 | ı | 7 | 5.7 | 7 | ı, | 6.2 | 6.9 | 7.3 | 6.7 | 5.1 | 7.4 | 6.9 | 8.1 | 7 | 6.5 | 6.9 | 7.7 | 8.1 | 8.1 |
| NO ₃ (mg/L) | | 55 | 3.8 | ı | 5.8 | 0.4 | 1 | 78 | 19 | 22 | | 0.1 | 0.5 | 1.2 | 9.0 | 1 | 0.04 | ı | . 1 | | 0.7 | 1 | 9.4 | 0.5 | 70 | 0.04 | 0.4 | 0 | 0.04 | 0.1 | 0.3 | 0.2 |
| F (mg/L) | | 0.4 | ı | 0.5 | 0.5 | 0.3 | 0.3 | 0.7 | ı | 0.2 | | 0.1 | ı | , | ı | ı | 0.4 | ı | 0.3 | 0.5 | 0.3 | . , | 0.7 | 0.3 | ı | 0.7 | 6.0 | 0.4 | 0.1 | 0.1 | 0.1 | |
| Cl (mg/L) | | 42 | 23 | 34 | 33 | 40 | 41 | 45 | 30 | 13 | | 11 | 40 | 255 | 270 | 44 | 20 | 390 | 166 | 83 | 20 | 119 | 222 | 20 | 53 | 315 | 53 | 144 | 62 | 32 | 22 | 18 |
| SO ₄ (mg/L) | | 72 | 59 | 38 | 51 | 24 | 59 | 43 | 20 | 15 | | 9 | 25 | 1640 | 120 | 83 | 135 | 631 | 350 | 264 | 11 | 612 | 103 | 27 | 23 | 879 | 99 | 302 | 40 | 57 | 62 | 44 |
| HCO ₃ (mg/L) | | 466 | 298 | 271 | 329 | 248 | 240 | 285 | 290 | 357 | | 06 | 180 | 1 | 49 | • ∞ | 222.1 | 250 | 184 | 242 | 166 | 364 | 0 | 216 | 46 | 521.1 | 148 | 270 | 122 | 200 | 231 | 224 |
| Sr (mg/L) | | 1 | ı | 1 | 1 | , | ı | , | ľ | 1 | | ı | 1 | ı | ı | | ı | 1 | ı | ı | 1 | , | | | | , | 1 | 1 | ı | ı | ı | ï |
| K (mg/L) | | ı | ١, | | , | , | | , | , | | | S | | | ţ | 1, | 5.8 | | | ď | 4.8 | 9 | , | 1 | | 9 | . 1 | , | 6.9 | ∞ | 4 | , |
| Na K (mg/L) (mg/L) | | 45 | 18 | 47 | 20 | 25 | 5 6 | 32 | 53 | 6 | | 34 | 99 | 91 | | 33 | 50 | 232 | 66 | 20 | 27 | 23 | 65 | 70 | 28 | 103 | 25 | . 69 | 29 | 76 | <i>L</i> 9 | . 22 |
| Mg (mg/L) | | 46 | ∞ | 16 | 21 | 13 | 15 | ∞ | ∞ | 14 | | | 6 | | | | | | | | | | | | | | | | \sim | | | |
| | | 104 | | | | | | | 87 | | | 52 | 21 | | | | | | | | | | | | | | | | | 61 | | |
| Si ng/L) (| | 19 | 24 | 14 | 1 | 1 | | 15 | 22 | 19 | | 40 | 23 | 7 | | | 34 | 1 | | | | | | | 20 | | | | | 42 | | |
| Temp Si Ca (C') (mg/L) (mg/L | | | | | | | · . | 1 | 21 | 1 | ion: | 56 | 1 | | | | 27 | . • | 24 | 24 | 1 | ı | | 27 | 21 | , | | 24 | 25 | 24 | 56 | 24 |
| YR 1 | | 1978 | 1949 | 1942 | 1958 | 1957 | 1957 | 1972 | 1952 | 1972 | Format | 1980 | 1952 | 1946 | 1956 | 1953 | 1989 | 1955 | 1964 | 1964 | 1964 | 1966 | 1972 | 1965 | 1953 | 1981 | 1972 | 1964 | 1988 | 1980 | 1980 | 1953 |
| State well number | Alluvium: | 5853105 | 5862104 | | 5862205 | 5862206 | 5862207 | | 5864703 | 5864711 | Calvert Bluff Formation: | 5846304 | 5846601 | 5846606 | 5847102 | 5847402 | 5847701 | 5847702 | 5847703 | 5847704 | 5847705 | 5847706 | 5847708 | 5847905 | 5854203 | 5854515 | 5855103 | 5855105 | 5855201 | 5855504 | 5855704 | 5855706 |
| | j., | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

| Spec. cond. (m\O) | | 576 | 1 | 1080 | 1700 | 900 | 1 | 920 | 1050 | | 1840 | 2140 | 611 | ı | 809 | 1 | 1440 | 335 | 1 | 1 | 224 | 423 | 460 | 645 | 548 | 914 | 277 | 915 | 700 | ı | i Cy | 463 | 1 : |
|------------------------------------|----------------------------------|---------|---------|---------|---------|------------|---------|----------------|---------|---------------------|---------|---------|---------|---------|---------|---------|---------|---------|------------|---------|------------|---------|---------|------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| Total hardness (mg/L) | | 204 | 1 | 14 | 14 | 134 | 120 | 34 | 31 | | 430 | 552 | 152 | - | 143 | 11 | 1 | 104 | 104 | 96 | 33 | 93 | 140 | 219 | 183 | 390 | 75 | 315 | 287 | . 1 | , | 172 | 244 |
| Total alk (mg/L) | | 107.38 | 335.03 | 465.57 | 518.03 | 207 | 184 | 258 | 264 | | 81.97 | 108.2 | 32.79 | . 1 | 18 | 31.97 | 67.19 | 68.85 | 21.31 | 31.97 | 17 | 13 | 126 | 112 | 185.25 | 245.9 | 63.93 | 240.98 | 187 | , | | 200 | 200 |
| TDS (mg/L) | | 382 | 1 | 650 | 724 | 496 | 317 | 572 | 298 | | 993 | 1116 | 341 | ı | 282 | 166 | ı | 196 | 283 | 192 | 129 | 207 | 272 | 386 | 326 | 551 | 229 | 536 | 408 | • | • | 264 | 421 |
| Hd | | 6.9 | 1 | ∞ | 8.1 | · ∞ | 8.3 | 8.1 | 8.5 | | 7.7 | 7.2 | 6.5 | 6.1 | 5.8 | 5.8 | 7.6 | 6.3 | 7.4 | 5.7 | 5.3 | 6.1 | 6.5 | 8.9 | 7.5 | 6.7 | 9.9 | 7.4 | 7.8 | 7.4 | 7.3 | 7.4 | 7.3 |
| NO ₃) (mg/L) | | 21 | 25 | 0.5 | 0 | 0.1 | 0.04 | 0.4 | 1.2 | | 11 | 11 | 1 | | 0.4 | ı | • | 0.2 | - | 0.05 | 1 | · 0.4 | 0.04 | 0.04 | 1 | 0.7 | 0.2 | 0.5 | 0.4 | ı | 1 | 0.1 | 0 |
| F (mg/L) | | | ı | 0.4 | 0.7 | 0.1 | 0.1 | 0.7 | 0.3 | | 1 | ı | 0.1 | r' | 0.7 | , | ı | 0.1 | 0.4 | j. | 1 | 0.1 | 0.5 | 0.7 | 0.7 | 0.7 | 0.4 | 1 | 0.3 | ı, | | 0.4 | 0.4 |
| C1 (mg/L) | | 17 | 202 | 42 | 26 | 36 | 53 | 48 | 22 | | 490 | 580 | 132 | | 133 | 99 | 256 | 46 | 118 | 9/ | 43 | 98 | 49 | 29 | 56 | 83 | 42 | 85 | 37 | 1 | 1 | 27 | 25 |
| SO ₄ Cl (mg/L) (mg/L) (| | 124 | 120 | 21 | 48 | 145 | 52 | 145 | 152 | | 99 | 46 | 42 | 10 | 36 | 14 | 180 | 15 | 30 | 22 | 12 | 32 | 70 | 91 | 29 | 105 | 9 | 92 | 88 | 69 | 140 | 11 | 74 |
| HCO3 (mg/L) | | 131 | 364 | 268 | 632 | 253 | 224.5 | 315 | 315 | , | 100 | 132 | 40 | • | 77 | 39 | 87 | 84 | 5 6 | 36 | 21 | 16 | 153.8 | 136.7 | 526 | 300 | 78 | 294 | 228 | | | 244 | 244 |
| Sr (mg/L | | 1 | 1 | ı | ı | ı | ı | ı | | | 1 | , | | ı | , | ı | 1 | 1 | | ı | , | ı | | ŧ | ı | , | 1 | 1 | | ı | | , | r |
| K (mg/L) | | | 1, | 1.5 | 1.6 | ς. | 4.51 | ı | ı | | 1 | | 6.4 | , | | ı | ı | 3.7 | 2.8 | 1 | 1 | 9 | 3.8 | 4.2 | n | 3.2 | 1.5 | ı | 1 | . ! | 1 | 3.4 | |
| Na K Sr (mg/L) (mg/L) (mg/L) | | 34 | l÷. | 258 | 288 | 120 | 69.91 | 199 | 210 | | 194 | 198 | 45 | ı | 46 | 25 | • | 70 | 20 | 30 | 5 6 | 32 | 36 | 33 | 42 | 37 | 23 | 99 | 22 | • | | 78 | 49 |
| Mg (mg/L) | | 9 | j | 7 | 7 | 6 | 8.31 | \mathfrak{C} | m | | 48 | 50 | 11 | 1 | 10 | 5 | | 4 | 6 | 9 | n | 7 | 8.1 | 12 | 13 | 16 | 4 | 19 | 16 | ı | ١, | 10.6 | 12 |
| Ca (mg/L) | | 72 | 1, | 5 | ĸ | 39 | 34.51 | 6 | ∞ | | 93 | 139 | 43 | | 40 | 22 | | 36 | 27 | 27 | 6 | 26 | 43 | 89 | 52 | 130 | 24 | 95 | 68 | ı | , | 51.4 | 78 |
| [emp Si Ca (C') (mg/L) (mg/ | nt.): | 4 | 1 | 14 | 14 | 18 | 8.43 | 13 | 13 | | 42 | 28 | 42 | ! | | 21 | 1 | 30 | 30 | 12 | 5 6 | 10 | 34 | 52 | 20 | 53 | 36 | 34 | 44 | ı | ı | 13 | 36 |
| Temp (C°) (i | tion (co | 22 | | ı | 56 | 27 | , | . 62 | 76 | יי | 1 | , | ı | | | 1 | | 73 | | | | 22 | 52 | 5 6 | 1 | | | , | • | 1 | ı | 23 | 76 |
| YR | ıff Forma | 1953 | 1946 | 1966 | 1966 | 1980 | 1989 | 1977 | 1980 | Formation | 1950 | 1950 | 1955 | 1980 | 1972 | 1951 | 1950 | 1966 | 1943 | 1951 | 1967 | 1980 | 1989 | 1989 | 1966 | 1966 | 1967 | 1953 | 1978 | 1980 | 1980 | 1988 | 1946 |
| State well number | Calvert Bluff Formation (cont.): | 5861304 | 5861801 | 5862107 | 5862110 | 5862302 | 5862303 | 5862406 | 5862506 | Simsboro Formation: | 5846204 | 5846301 | 5846303 | 5846410 | 5846501 | 5846502 | 5846503 | 5846508 | 5846509 | 5846510 | 5846511 | 5846512 | 5846516 | 5846611 | 5846707 | 5847109 | 5853809 | 5853905 | 5854205 | 5854305 | 5854306 | 5854403 | 5854501 |

| YR | Temp (C°) | Si (mg/L | Femp Si Ca (C°) (mg/L) (mg/L) | Mg (mg/L) | Na (mg/L) | Na K Sr (mg/L) (mg/L) (mg/L) | Sr (mg/L) | HCO3 (mg/L) | SO ₄ (mg/L) | SO ₄ Cl (mg/L) | F (mg/L) | F NO ₃ (mg/L) (mg/L) | Hd | TDS (mg/L) | Total Total alk hardness (mg/L) (mg/L) | Total ardness (mg/L) | Spec. cond. |
|-----------------------------|--------------|-------------|----------------------------------|--------------|--------------|---------------------------------|--------------|---------------------------------------|------------------------|---------------------------|-------------|---------------------------------|----------|------------|--|----------------------|----------------|
| Simsboro Formation (cont.): | £ . |) | | • | | | D | | h h | | À |) A | |) h | | | |
| 1946 27 | | 1 | 78 | | 47 | ı | , | | 89 | 54 | 0.4 | | 7.4 | 374 | 103 44 | 240 | |
| 1980 27 | | 41 | 95 | , ∞ | 32 | ı | 1 | 231 | 25 | 52 | 0.3 | 0.1 | 7.7 | 415 | 189 | 270 | 735 |
| | | | 99 | | 61 | 1 | . 1 | | 74 | 9 4 | 0.4 | 0 | 7.3 | 381 | 199.18 | 214 | , ' |
| 1946 27 | | ı | 89 | | 89 | | | | 85 | 55 | 0.4 | 0 | 7.2 | 407 | 199.18 | 219 | ٠ |
| - 5761 | | | . 87 | | 56 | ı | , | | 71 | 40 | 0.3 | · ∞ | ! | 361 | 195 | 266 | 1 |
| 1944 - | | ı | 81 | | 30 | ı | ı | | 59 | 39 | 0.4 | 0.4 | 7.3 | 341 | 200 | 252 | |
| 1942 - | | 1 | 74 | | 32 | | - 1 | | 61 | 48 | | , | ı | 327 | 168.85 | 230 | • |
| 1980 - | | ı | • | | | ı | | ٠, | 2000 | 1 | 1 | 1 | 9.9 | ٠ | 1 | 1 | ٠ |
| 1993 27 | | 35 | 88 | | 28 | 3.4 | 0.46 | | 99 | 41 | 0.24 | 0.04 | 7.1 | 381 | 182 | 261 | 591 |
| 1953 - | | 78 | 82 | | 20 | ı | | | 30 | ∞ | | 0.2 | 7.8 | 320 | 240.98 | 238 | 556 |
| - 1961 | | 53 | 46 | | 5 6 | 3.6 | | | 15 | 28 | 0.3 | 0.7 | 7 | 235 | 137.7 | 135 | 384 |
| | | 23 | 22 | | 33 | 3 | | | 45 | 27 | 0.2 | 0.4 | 8.3 | 295 | 168 | 171 | 504 |
| | | 22 | 35 | | 121 | ı | | | 0 | 42 | 0.2 | 0.1 | 7.8 | 408 | 307 | 105 | 750 |
| 1993 36 | | 22 | 12 | | 08 | 3.4 | 1.11 | | 23 | 12 | 0.18 | 0.04 | ∞ | 263 | 176 | 47 | 362 |
| 1953 - | | 46 | 148 | | 65 | , | 1 | | 80 | 214 | | 0.4 | 6.9 | 704 | 214.75 | 460 | 1230 |
| 1956 - | | ı | | | 1 | 1 | 1 | | 1 | 24 | | 1 | 6.9 | • | 101.61 | 1 | 737 |
| 1960 - | | 36 | 106 | | 41 | ı | , | | 260 | 18 | ι—, | 0 | 6.3 | 543 | 112.3 | 322 | 756 |
| | | | 7 | | 256 | 1 | 1 | | 103 | 28 | 0.4 | 0.04 | 8.6 | 665 | 398 | 24 | 1215 |
| | | 14 | 5.9 | | 279 | 3.4 | , | | 82 | 54 | 0.3 | 0.04 | 8.2 | 700 | 431 | 53 | 1100 |
| 1993 26 | | 14 | 3.9 | | 340 | 3.7 | 0.36 | | 36 | 107 | 1.24 | 0.04 | 8.5 | 839 | 552 | 18 | 1223 |
| - 9861 | | , | cc | | 432 | | | | 4 | 279 | 2.3 | 0 | 8.3 | 1053 | 554 | 14 | 1800 |
| Ī | | | 4 | | 325 | 1 | | | 26 | 81 | 1.4 | 0.04 | 9.1 | 804 | 559 | 19 | 1485 |
| Hooper Formation: | | | | | | | * | · · · · · · · · · · · · · · · · · · · | ٠ | | | | | | | | |
| - 0561 | | 34 | 18 | 7 | . 89 | | , | 139 | 15 | 26 | 1 | 7 | 7.9 | 281 | 113 93 | 73 | 462 |
| 1983 - | | 43 | 62 | | 29 | | | 149 | 29 | × 5 | 0.2 | 0 | 7.7 | 331 | 122 | 202 | 525 |
| 1950 23 | | ۱ ؛ | ' | ¦ ' | ' | , | 1 | 233 | 120 | 240 | 1 |) ' | × 4 | , ' | 222.59 | } ' | 1400 |
| | | 53 | 222 | 42 | 117 | , I: | , | 422 | 213 | 294 | 0.3 | 1.3 | 7.4 | 1126 | 346 | 730 | 1740 |
| 1950 - | | 32 | 70 | 15 | 51 | | , | 248 | 22 🍦 | 98 | y I | 0 | 8.2 | 397 | 203.22 | 236 | 691 |
| 1950 - | | 12 | 165 | 89 | 258 | , 1 | 1 | 334 | 191 | 550 | | 3.5 | 7.4 | 1411 | 273.69 | 691. | 691 |
| 1950 - | | 71 | 9 ! | 4 ; | 57 | | t | 115 | 14 | 24 | 0 | 14 | 8.9 | 246 | 94.26 | 30 | 316 |
| 1 | | 36 | 43 | 13 | 169 5 | í | | 201 | 83 | 197 | 1 (| 1 (| 7.2 | 642 | 164.75 | 161 | 1140 |
| 1980 25 | | 40 | 110 | 7 | 74 | 1 | , L | 55/ | 97 | | 0.7 | 0.1 | 9./ | 445 | 276 | 281 | 648 |
| | | | | | | | | | | | | | | | | | |

Table 2 (cont.)

| Spec. cond. | (mQ) | | 952 | 592 | 775 | 778 | • | • | 1 | 548 | 1057 | • | 1 | 1170 | 700 |
|-------------------|-------------------|---------------------------|---------|---------|---------|----------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| Total hardness | mg/L) | | 304 | 223 | 392 | 1 | i | ı | 229 | 207 | 39 | ı | ı | 74 | 236 |
| Total alk | (mg/L) (1 | | 218.03 | 210 | 239 | | | • | 193 | 199 | 1 | 191.75 | 304.83 | 323 | 230 |
| TDS | (mg/L) | | 532 | 383 | 514 | ٠ | • | ! | 389 | 337 | 573 | 1 | 1 | 729 | 391 |
| Hd | | | 7.2 | 7.7 | 8.5 | 8.8 | 7.4 | 7.1 | 8.1 | 7.7 | 8.3 | , | | , | 9.7 |
| | (mg/L) | | 21 | 0.1 | 0.1 | ı | 1 | 1 | 1 | 0.04 | e | 41 | 12 | 2.5 | 0.04 |
| ΙΉ | (mg/L) | 6 | 0 | 0.3 | 0.1 | 1 | 1 | 1 | 1 | 0.44 | 0.3 | 1 | 1 | 0.5 | 0.2 |
| ご | (mg/L) | | 144 | 89 | 130 | ∞ | ı | • | 88 | 39 | 125 | 69 | 52 | 216 | 90 |
| SO ₄ | (mg/L) | | 22 | 27 | 31 | 33 | 69 | 30 | 22 | 23 | 16 | 100 | 20 | 5 | 17 |
| | (mg/L) (| | 266 | 256 | 277 | 398 | 1 | 1 | 235 | 242.9 | 381 | 234 | 372 | 394 | 280.6 |
| Sr | (mg/L) | | | , | | 1 | 1 | | • | 0.44 | 1 | | . 1 | • | ı |
| × | (mg/L) | | , | ı | 1 | , | 1 | 1 | • | 3.7 | , | , | , | • | 4.5 |
| Na | ng/L) | | 72 | 52 | 24 | | | | 51 | 40 | 214 | | | 256 | 43 |
| Mg | L) (mg/L) (n | | 17 | 11 | 10 | , | 1 | , | 12 | 11 | т | ı | , | 7 | 13.9 |
| Ca | (mg/L) | | 94 | 71 | 140 | ı | | , | 72 | 65 | 10 | 1 | | 18 | 71.5 |
| Si | mg/L) | | 32 | 28 | 36 | , | | | 53 | 35 | 15 | ı | , | 31 | 13 |
| Temp Si | (C°) (mg/L) (mg/I | cont.): | 1 | 24 | 25 | ı | . 1 | , | ı | 56 | 56 | 22 | 22 | • | 25 |
| | YR | mation (| 1950 | 1980 | 1980 | 1966 | 1980 | 1980 | 1970 | 1993 | 1980 | 1946 | 1946 | 1974 | 1988 |
| State well | number | Hooper Formation (cont.): | 5846207 | 5846208 | 5846211 | 5846402 | 5846413 | 5846504 | 5846513 | 5846515 | 5854706 | 5860307 | 5860308 | 5861110 | 5861206 |

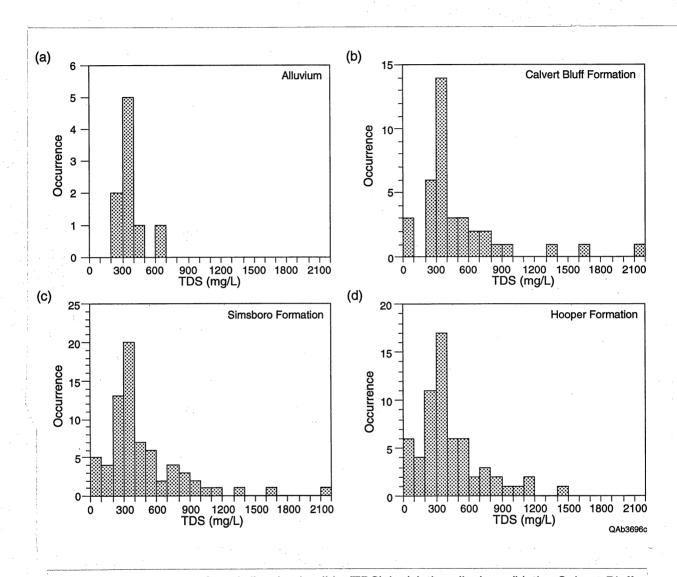


Figure 12. Histograms of total dissolved solids (TDS) in (a) the alluvium, (b) the Calvert Bluff Formation, (c) the Simsboro Formation, and (d) the Hooper Formation of Bastrop County.

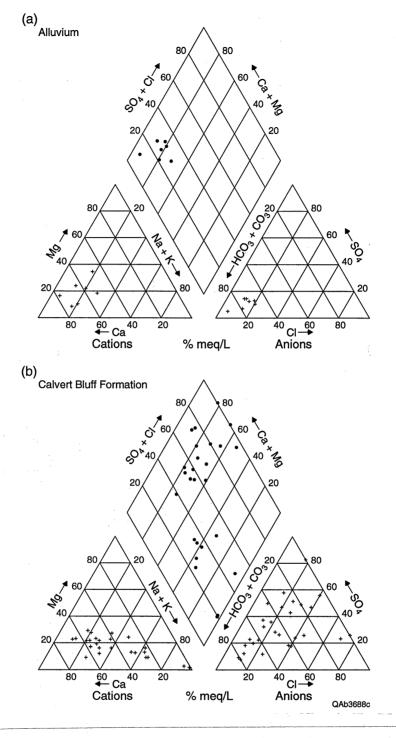


Figure 13. Trilinear diagram showing chemical composition of ground-water samples from the (a) alluvium and the (b) Calvert Bluff Formation in Bastrop County.

Waters from the Simsboro Formation are a mixed calcium and sodium-bicarbonate type with some sodium-chloride type waters (fig. 15a). Waters from the Hooper Formation are a calcium-bicarbonate with some sodium-chloride type waters (fig. 15b).

Powell Bend Mine, located just southwest of the camp, has several wells penetrating the Simsboro that have quarterly water-chemistry data since 1987 that we culled from RRC files (app. 3). These data document temporal variations in water quality in these wells. The site geologist suggested that the mine never affected water quality in the Simsboro (mining of coal was in the Calvert Bluff). There are, however, some interesting variations in water quality that are perhaps related to recharge events because these wells are of limited depth (~100 ft). These data should be considered semiquantitative because of the nonideal collection and analysis methods.

Results from the chemical analyses on ground water collected from the Camp Swift monitor wells are shown in table 3. Water from SWIFT-1 is a sodium-bicarbonate type, whereas water from SWIFT-2 is a mixed-cation-chloride type.

Conceptual Flow Model

A conceptual flow model is a hypothesis of ground-water flow based on the available hydrogeologic information. The following conceptual ground-water flow model is based on the geology and topography of Camp Swift and surrounding area, water-level measurements in wells on and around the camp, and hydrologic properties measured as part of this study and reported in previous investigations. According to this model, rain falls on the outcrop of the Calvert Bluff Formation and a small percentage percolates into the ground to recharge the shallow unconfined aquifer. Recharge to the aquifer is greater at higher elevations and in sandier patches of the outcrop. This water moves from topographic highs toward topographic lows where it discharges to local creeks and streams. Some of the ground water follows longer flow paths and discharges into locally major topographic lows such as Big Sandy Creek and Dogwood Branch. A small amount of ground water moves parallel to bedding and continues downdip toward the east. There also may be flow from the Calvert Bluff Formation into the underlying Simsboro Formation, especially near the Sayersville Fault.

Ground-water flow in the Simsboro Formation is from the east toward the west beneath Camp Swift. Recharge for the Simsboro Formation is mainly derived from the outcrop east of Camp Swift, though lesser amounts of water may come from the Calvert Bluff Formation by cross-formational or cross-fault flow. A schematic of our conceptual model is shown in figure 16.

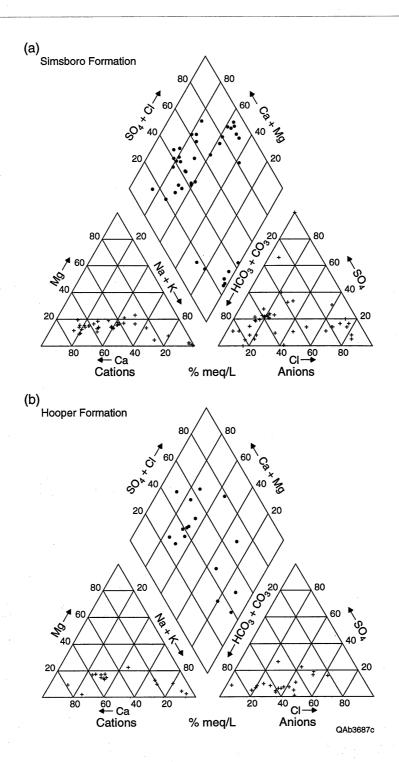


Figure 14. Trilinear diagram showing chemical composition of ground-water samples from the (a) Simsboro and the (b) the Hooper Formations in Bastrop County.

Table 3. Chemical analyses of ground water from Camp Swift monitor wells (mg/L).

| SWIFT-1 | SWIFT-2 |
|---------|---|
| 6.0 | 6.1 |
| 20.8 | 17.6 |
| 33.2 | 909 |
| 7.7 | 12.0 |
| 3.6 | 338.9 |
| 13.2 | 830.0 |
| 24.5 | 1964.0 |
| 0.4 | 4.9 |
| 0.3 | na |
| 24.9 | 2143.0 |
| 79.1 | 156 |
| 5 (4) | |
| | 6.0 20.8 33.2 7.7 3.6 13.2 24.5 0.4 0.3 24.9 79.1 |

na = not analyzed (n) = 1 standard deviation of tritium counting data

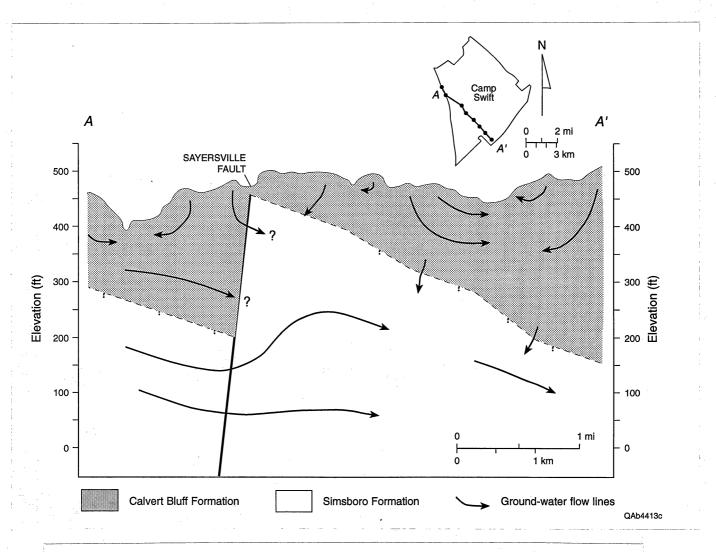


Figure 15. Schematic of the conceptual ground-water flow model for Camp Swift. Cross section after Gaylord and others (1985).

SURFACE-WATER HYDROLOGY

Principal Streams and Watersheds

Camp Swift resides in the Colorado River Basin (zone 3; TDWR, 1983). The northern part of the camp is drained by Big Sandy Creek and its tributaries, which include Dogwood Creek, McLaughlin Creek, and various unnamed creeks. McLaughlin Creek collects runoff from the northeastern half of the camp and empties into Big Sandy Creek in the northwest part of the camp. The southern part of the camp is drained by Dogwood Branch and to a lesser degree by a tributary to Harris Creek, both of which empty into Big Sandy Creek west of the camp. Big Sandy creek ultimately empties into the Colorado River.

Most of Camp Swift lies in the Big Sandy Creek watershed, which includes the Dogwood Creek, McLaughlin Creek, and Dogwood Branch subbasins (fig. 17). A very small part of the camp in the southeast is included in the Piney Creek watershed (fig. 17).

Stream-flow Duration and Flood Frequency

There is one currently operating stream gauge just outside Camp Swift on Big Sandy Creek. Big Sandy Creek has flows as high as 2,400 cubic feet per second (cfs) (fig. 18a). Big Sandy Creek flows 85 percent of the time (fig. 18b). Using a Log Pearson Type III fit to the annual maxima series, there is a 50-percent chance of having an annual flood greater than 1,200 cfs in Big Sandy Creek (fig. 18c). Stream-flow characteristics of Big Sandy Creek are summarized by U.S. Department of the Interior (1980), Gaylord and others (1985), and Avakian and Wermund (1993). U.S. Department of the Interior (1980, table 2-7, p. A4-5–A4-8) estimated the 100-yr flow at Big Sandy Creek on the west side of the camp to be 20,850 cfs, at the mouth of McLaughlin Creek to be 6,780 cfs, and where Dogwood Branch crosses Highway 95 to be 4,470 cfs.

Floodplain Analysis

FEMA (1991) published flood hazard boundaries for Big Sandy Creek, McLaughlin Creek, Dogwood Creek, and their tributaries. We transferred the FEMA (1991) floodplains to USGS 1:24,000 topographic sheets and better constrained the floodplains on the tributaries (fig. 19). Flooded areas are generally confined to the drainages of creeks on the camp (fig. 19). Flooding adjacent to Dogwood and McLaughlin Creeks would be relatively minor. Larger areas adjacent to Big Sandy Creek would be flooded following a major storm, especially at lowlying confluence points.

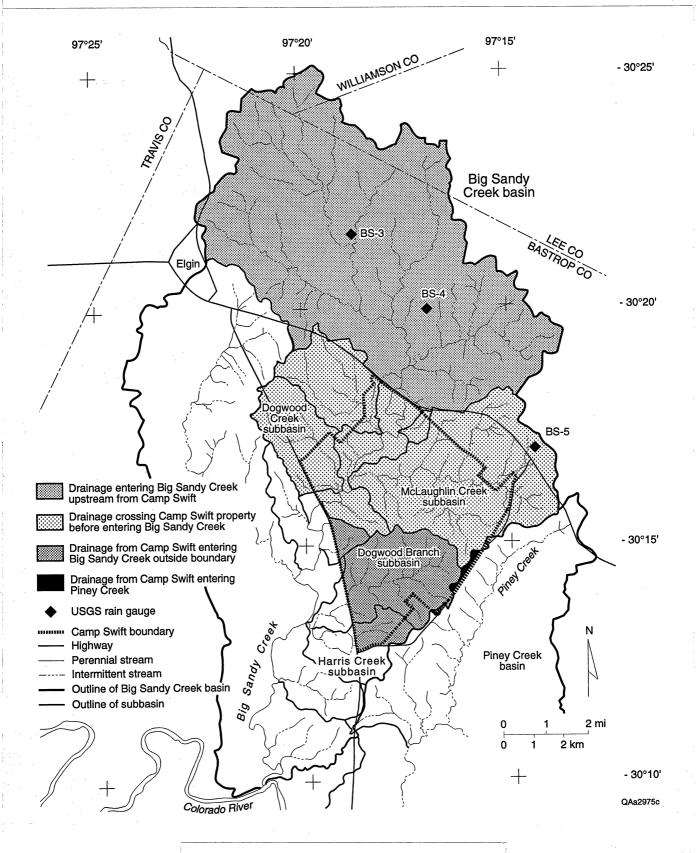


Figure 16. Watershed delineations for Camp Swift.

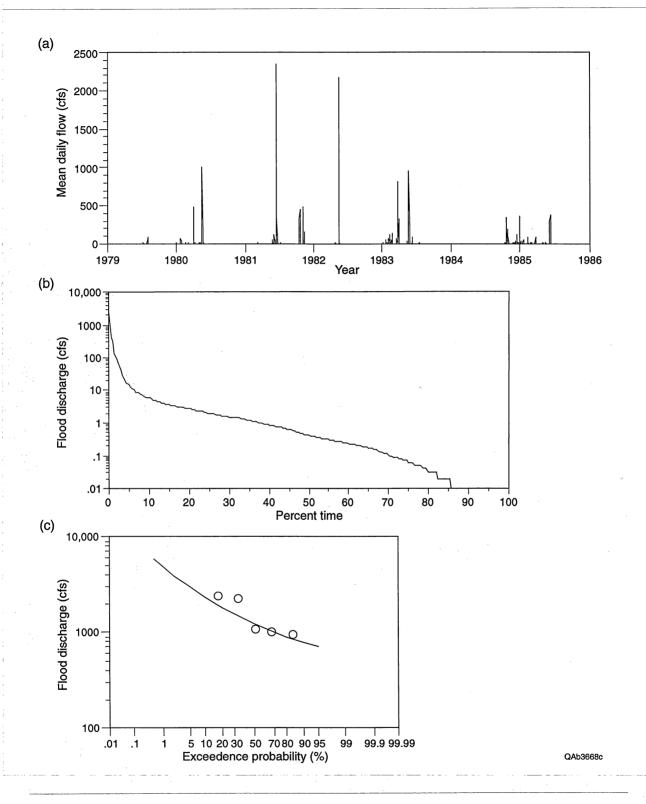


Figure 17. (a) Mean daily flow, (b) flow duration, and (c) flood frequency analysis with a log Pearson Type III fit for a stream gauge on Big Sandy Creek near Elgin.

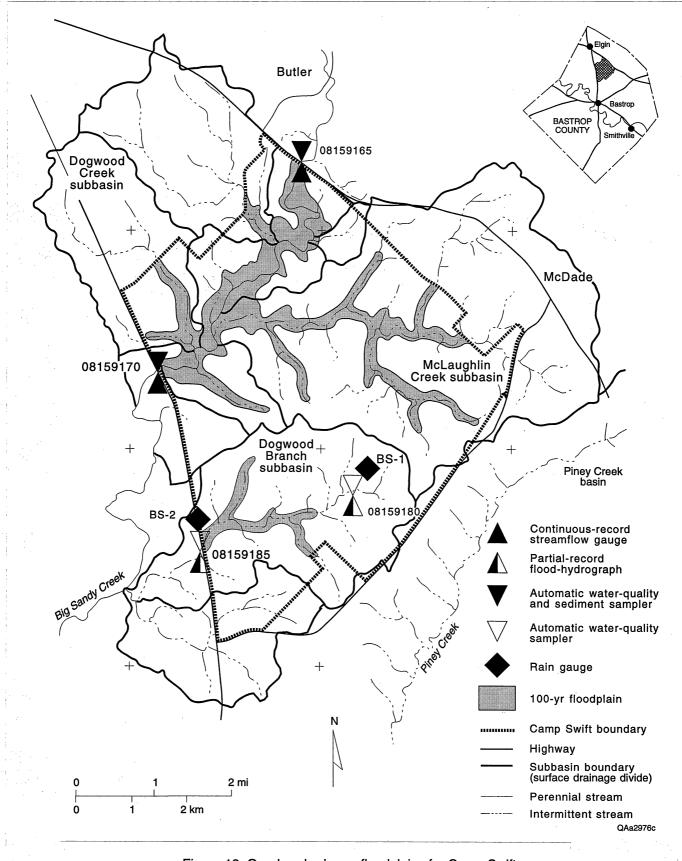


Figure 18. One-hundred-year floodplains for Camp Swift.

GIS DATA PREPARATION

Several layers of data and information were automated for inclusion into a geographical information system (GIS). These layers include:

- Roads
- Watersheds
- Digital elevation map (DEM)
- Floodplains
- Soil maps
- Location of off-camp wells
- · Location of on-camp wells
- Water-level maps

The data dictionary for these layers is included in appendix 4.

SUMMARY

The hydrogeologic survey located 83 ground-water wells around Camp Swift and 7 wells on the camp grounds. Eight potential well sites on Camp Swift were identified, but wells were not found. Ground water is pumped from near-surface alluvium and from strata within the Wilcox Group, primarily the Hooper, Simsboro, and Calvert Bluff Formations. Water levels in wells from the Hooper and Simsboro Formations show a gradual rise following dry periods in the 1950's, whereas water levels in shallower strata show fluctuations but no long-term trends. Ground-water recharge is primarily from precipitation on topographically high regions where the Calvert Bluff Formation is exposed and in the more sandy parts of the camp. This water percolates downward toward topographically low regions where it discharges to local creeks or streams. A small amount of recharge probably continues down stratigraphic dip to the east. Some flow from the Calvert Bluff Formation to the Simsboro Formation may also occur, primarily near the Sayersville Fault that cuts through the camp from northeast to southwest. Ground-water quality is fresh to brackish. Calcium-bicarbonate, sodium-bicarbonate, calcium-sulfate, and sodium-chloride water types are produced from wells on and near Camp Swift.

The northern part of the camp is drained by Big Sandy Creek and its tributaries Dogwood Creek, McLaughlin Creek, and several unnamed creeks. The southern part of the camp is drained primarily by Dogwood Branch and other, smaller tributaries, all of which flow into Big Sandy Creek west of the camp and ultimately to the Colorado River. Most of Camp Swift is in the Big Sandy Creek watershed, which includes the Dogwood Creek, McLaughlin Creek, and Dogwood Branch subbasins. A 100-yr flood would submerge small areas adjacent to McLaughlin Creek and Dogwood Branch, with wider flooding in the west-central and northern parts of the training facility where stream valleys are wider.

Chemical contamination or spills on recharge areas are the principal threats to ground-water quality on Camp Swift. Such contamination, particularly on sandy, topographically high exposures of the Calvert Bluff Formation could be transported downward to the shallow, unconfined aquifer system. Chemical contamination or debris in streambeds or floodplain areas are the principal threats to surface-water quality because they may be washed into the surface-water system during or after heavy rainfalls.

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Appendix 1 Well Inventory Data Base

| base. |
|--------------------------|
| v data |
| pendix 1. Well inventory |
| . Well |
| endix 1 |
| ā |

| | | | ** _{\$\infty\$} | | Append | IX 1. Well II | Appendix 1. Well inventory data base | ġ. | | Land-surface |
|--------------|------------|---------|--------------------------|------------------------------------|----------|---------------|---------------------------------------|---------------------------------------|---------------|--------------|
| Well | Well Cond. | Depth | Water level | Water level Casing height Diameter | Diameter | Casing | Well | | Topographic | elevation |
| 0 | (DII) | (ft) | (ft BTOC) | (ft) | (inches) | material | esn | Owner | quadrangle | (ft) |
| S001 | | , | 1 | ı | 1 | | water supply | Aqua Water | Lake Bastrop | ı |
| S00 2 | | | 1 | | • | • | ı | | Lake Bastrop | |
| S003 | • | ~600 | 160.02 | 1.00 | 4 | PVC | domestic | Parma | Lake Bastrop | 487 |
| S004 | 725 | 1 | 1 | | • | | domestic | | Lake Bastrop | , |
| S005 | | 1 | | • | 4 | N S | • | | Lake Bastrop | • |
| 900S | | 1 | ı | • | • | • | | • | Lake Bastrop | 496 |
| 2002 | | 969 | ı | • | | ı, | domestic | | Smithville NW | 528 |
| 8008 | | | | • | | | domestic | • | Smithville NW | |
| 800S | | | *** | | • | | • | ı | Lake Bastrop | |
| S010 | | ı | | • | | | • | Powell Bend Mine | Lake Bastrop | • |
| S011 | | ~200 | 47.12 | 0.28 | 4 | PVC | pesnun | Ray Shannon | Lake Bastrop | 418 |
| S012 | 650 | | • | • . | | • | · | Steiner Ranch | Lake Bastrop | i |
| S013 | , | 1 | • | • | | • | | | Lake Bastrop | |
| S014 | • | ı | , | • | | | | | Elgin East | ı |
| S015 | | į | | • | | | • | Kenneth Wilson | Elgin East | ı |
| S016 | | 1 | ı | • | | | | | Elgin East | 1 |
| S017 | | | ١,, | | • | , | | 1 | Elgin East | |
| S018 | | *, • | | • | | , | , , , , , , , , , , , , , , , , , , , | | Elgin East | 1 |
| S019 | 250 | ~65 | ~59 | 1 | 36 | | stock water | 1 | Elgin East | • |
| S020 | ı | 1 | ı | | | | | • | Elgin East | |
| S021 | | ī | | 1 | | | | | Elgin East | 1 |
| S022 | | 126 | | • | | • | pesnun | Mrs. Hughes | Elgin East | , |
| S 023 | | ~100 | dry | • | ~48 | | • | Mrs. Hughes | Elgin East | • |
| S024 | | 165 | ~65 | • | | | ı | * * * * * * * * * * * * * * * * * * * | Elgin East | • |
| S025 | , | ~65 | ~45 | 1 | • | | 1 | | Elgin East | • |
| S 026 | | | • | • | • | | 1 | | Elgin East | • |
| S027 | | 3, | • | | • | | | • | McDade | , |
| S028 | 220 | 692 | 170.93 | 1.48 | <u>ග</u> | P | domestic | Charles Stanley | McDade | 268 |
| S 029 | | • | • | 1 | • | | ı | Arthur Mundine | Smithville NW | • |
| S030 | | ~97-100 | 38.73 | 0.00 | က | P.C | pesnun | Arthur Mundine | Smithville NW | 540 |
| S 031 | | | • | 1 | • | 1 | | Arthur Mundine | Smithville NW | • |
| S032 | | ı | • | • | • | | plugged | UT Env. Sci. Park | Lake Bastrop | • |
| S033 | | | • | 1 | 4 | | plugged | UT Env. Sci. Park | Lake Bastrop | • |
| S 034 | | ı | • | | | `\ | plugged | UT Env. Sci. Park | Lake Bastrop | • |
| S035 | | ı | • | ı | `I | | filled in | | Lake Bastrop | • |
| S036 | , | ~110 | • | 1 | | | ī | | Lake Bastrop | 520 |
| S037 | | | • | 1 | | | 1 | | McDade | |
| | | | | | | | | | | |

Appendix 1. Well inventory data base.

| Depth (ft) ~400 | | Water level Casing height Diameter Casing (ft BTOC) (ft) (inches) materia | Casing height (ft) | Diameter (inches) | Casing material | meter Casing Well ches) material use | Owner | Topographic quadrangle McDade | Land-surface elevation (ft) |
|-----------------------|------------|---|--------------------|----------------------|--------------------|--------------------------------------|-------------------|-------------------------------------|-----------------------------------|
| | • | • | | | , | • | • | McDade | |
| | | | | ٠. | | • | • | McDade | • |
| | 1 | | | | | | • | McDade | |
| | • | • | | • | , | • | • | McDade | • |
| | 1 | • | | 1 | ı | domestic | • | McDade | 480 |
| ~80 flowing | flowing - | ι, | | 1. | | • | .• | McDade | 460 |
| 126 | | | | • | | • | • | McDade | • |
| 1 | • | • | | | ١. | • | 1 | Smithville NW | ı |
| | 1 | Ī | | • | 1 | • | • | Smithville NW | ı |
| | | | | | 1 | • | • | Smithville NW | • |
| | 1 | • | | | | • | • | Smithville NW | • |
| - 36.05 1.83 | _ | 1.83 | | ~30 | brick | pesnun | • | McDade | 551 |
| | | | | 1 | 1 | ı | • | McDade | • , |
| 1 | 1 | 24 | | | | • | • | McDade | |
| | 1 | • | | 1 | 1 | • | • | McDade | • |
| • | 1 | • | | • | į | • | Ray Edwards | McDade | • |
| 250 57.88 0.18 | 0. | | | 4 | PVC | garden | Duggars | Elgin East | 480 |
| | 1 | | | | | • | • | Elgin East | • |
| 484 | | | | 4.5 | | domestic | Aqua Water Supply | Elgin East | • |
| 1 | | | | | 1 | • | 1 e., | Elgin East | `• |
| | 1 | 1 | | 1 | ı | nursery | • | Elgin East | 1 |
| 725 | 1 | 1 | | 4 | ı | domestic | Aqua Water Supply | Elgin East | |
| 642 | | | | 4.5 | 1 | domestic | Aqua Water Supply | Elgin East | • |
| 202 | 1 | • | | 4.5 | ı | domestic | Aqua Water Supply | Elgin East | ı |
| 1558 | | , | | 2 | | domestic | Aqua Water Supply | Smithville NW | |
| | 1 | • | | 1 | ı | | Aqua Water Supply | Lake Bastrop | |
| | | | | • | Ī | • | Aqua Water Supply | Lake Bastrop | • |
| | | | | • | Ī | ı | Aqua Water Supply | Lake Bastrop | • |
| 197 47.12 0.28 | 47.12 0.28 | 0.28 | | 4 | PVC | garden | Fay Pannell | Lake Bastrop | 415 |
| ~50-60 dry 2.50 | | 2.50 | | • | concrete | • | Fay Pannell | Lake Bastrop | 405 |
| | 1 | | | • | • | domestic | Bill Walton | Elgin East | • |
| ~110-120 ~90 - | - 06~ | ı | | • | ı | • | • | Elgin East | 544 |
| 1 | | | | • | | • | • | Elgin East | |
| 1 | | | | 1 | • | • | • | Elgin East | ı |
| 1 | | | | | | • | | Elgin East | • |
| 1 | | • | | • | | , | • | Elgin East | |
| | | | | | | | | | |

Appendix 1. Well inventory data base.

| Land-surface | elevation | (ft) | 13 | 505 | 484 | • | • | • | • | 502 | ı |
|--------------|---|-------------------|------------|-------------|------------|-------------|---------------------------------------|------------|------------|------------|------------------------|
| | Topographic | quadrangle | Elgin East | Elgin East | Elgin East | Elgin East | Elgin East | Elgin East | Elgin East | Elgin East | Lake Bastrop |
| | | Owner | • | Earl Hold | Stagner | | J. L. Christensen | • | • | Zane Cole | Fay Pannell's daughter |
| | Well | asn | - | domestic | lawn | • | | ı | • | nunsed | domestic |
| | Casing | material | | PVC | | | • | • | | iron | PVC |
| | Diameter | (inches) material | | 4 | | • | • | • | • | 4 | 4 |
| | Vater level Casing height Diameter Casing | (ft) | ı | 0.43 | | • | 1 | • | , | 0.58 | • |
| | Water level | (ft BTOC) | | 35.58 | ~20 | ı | ı | 1 | 1 | 52.83 | |
| | Depth | (ft) | 40 | ~50-60 | 80 | | , | 100 | 100 | 80 | 525 |
| | | (дд) | ١, | | | | | | | | |
| | Well | no. | S075 | S076 | S077 | S078 | 8079 | S080 | S081 | S082 | S083 |

All depths reported by owners

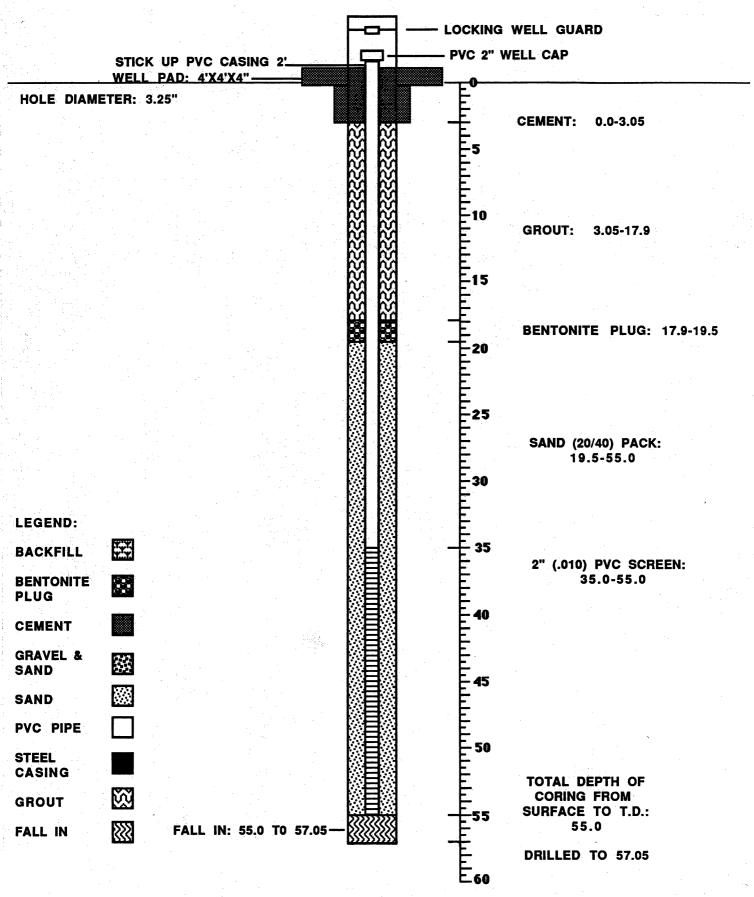
~ indicates owner-supplied information
BTOC = below top of casing
Land-surface elevations estimated from USGS topographic maps

Appendix 2

Well Schematics and Drilling Reports for Monitor Wells

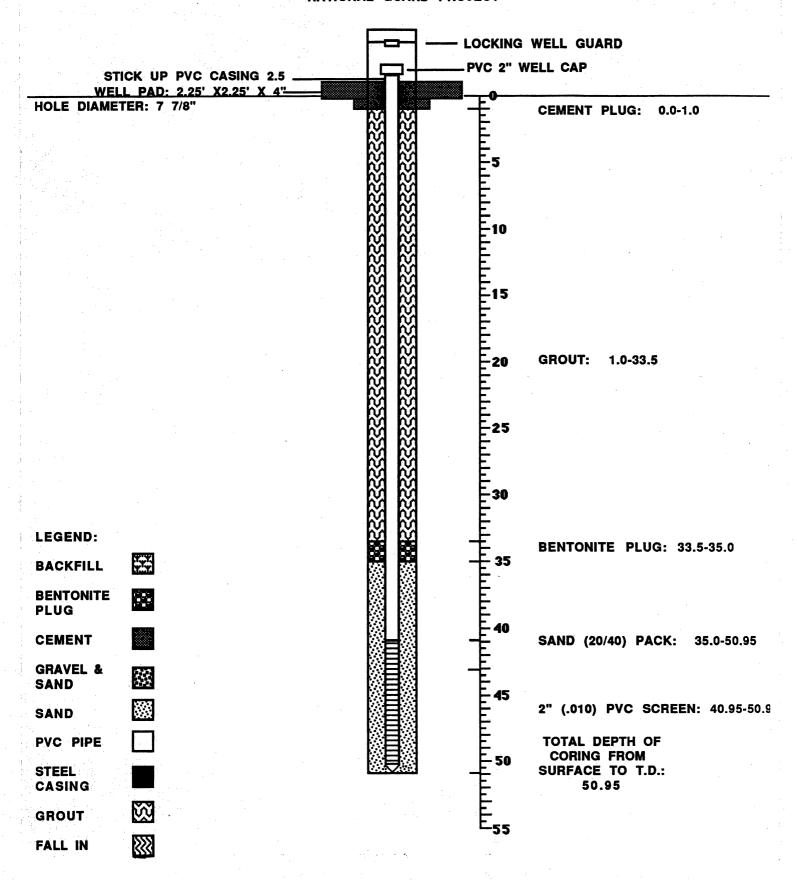
| ATTENTION OWNER: Confidentiality Privilege Notice on Reverse Side | | State of WELL RE | EPO | RT | | | ter Well Drill P.O. Box Lustin, Texas 512-239 | c 13087 : 78711-3081 | · . |
|---|---|------------------|----------|-----------------|--------------------------------|---------------------------------------|--|-------------------------|---------------------------------------|
| | | Camp S | WIL] | | | | | _ | |
| 1) OWNER Texas Natio | | ADDRESS | | P.C |). Box 5218 | Aust | | · | 78763 |
| M ADDEDO OF UP! | (Name) | - - | | | (Street or RFD) | (City | 7) | (State) | (Zip) |
| 2) ADDRESS OF WELL: County Bastrop | Camp Swift Rt. 2, Box 151 | -X Ba | stro | р | Texas | s 78602-973 | 7 GRID | #58 | -46-8 |
| Dastrop | (Street, RFD or other) | | City) | | (State | | | | |
| | | | | | Engles | all Borine | patic | 5) | A. |
| 3) TYPE OF WORK (Check): | 4) PROPOSED USE (Check): | _ | | _ | Environmental Sc | oll Boring □ Dorr -watering ☑ Test | • | 200 47 | 14" |
| New Well □ Deepening | | on 🗆 Injection | | | | · . | | 30° 17 | |
| ☐ Reconditioning ☐ Plugging | If Public Supply well, were p | pians submitted | to the | e INRC | C? Yes | □ No | | 97° 18' | 26" |
| 6) WELL LOG: | DIAMETER OF HOLE | | 7) | DRILL | ING METHOD (C | check): Driv | ren | | |
| Date Drilling: | Dia. (in.) From (ft.) | To (ft.) | | _ | | Aud Rotary 🗆 Bore | _ | | |
| Started 10/31 19 95 | 3 1/4 Surface | 57.05 | | | - T | Cable Tool | Den | | .1 |
| Completed 11/1 19 95 | | | | Ø Ot | | | | | N |
| Emm /6 \ T_ /6 \ | Description and color of formation | ı material | g) | Boreh | ole Completion | (Check): 🗆 O | pen Hole | ⊠ Straigh | nt Wali |
| From (ft.) Το (ft.) Ν/Δ | Rock Bitted | | -1 | | | ☐ Gravel Packed | ☐ Other _ | | <u> </u> |
| INVA | , IOOK DILLOU | | | | | - | ft. | to | |
| | | | | | | nterval from | | | |
| | | | CAS | New New | Steel, Plastic | D WELL SCREEN DA | | ng (ft.) | Gage |
| | | | Dia | or | Perl., Slotted | , etc. | | | Casting |
| | | | (in.) | Used | | if commercial | From 2 Above | To | Screen |
| | | | 2" | N. | | <u>dule 40 - 40'</u> | Surface | 35.0 ' | |
| | | | 2" | N | PVC Sche | dule 40 - 20' | 35.0' | 55.0' | .010 |
| | | | | | | | | | |
| | | | | | | | | <u> -</u> | |
| | | | 9) | CEME | NTING DATA: | [Rule 338.44(1)] | | | 1 V 1 |
| | | | | | | | | | |
| | | | | Came | 4" Above inted from Surface | n. to 3.05 n. | No. of Sack | s Used | 4 |
| Y Commence of the Commence of | | | | -911 R J | | ft. to tt. | No. of Sack | | |
| | | | | k # - ** | | | UI SACI | | |
| | | | | | dused Hand P | | | | |
| | | | | | nted by Drill Cr | | | | |
| (Use reve | rse side if necessary) | · | | | | em field lines or other | | contaminati | on N/A f |
| 13) TYPE PUMP: | | | <u> </u> | Metho | d of verification o | of above distance N | Ά | | · . |
| | Submersible Cylinder | 1 | 10 | | FACE COMPLET | | | - | |
| ☐ Other | | <u> </u> | , | | | | 200 44 40 4 | W. | |
| Depth to pump bowls, cylinder | r, jet, etc., | ft. | | . — | • | Slab Installed [Rule | | | |
| | | | | × | Specified Steel S | leeve Installed [Rule | 338.44 (3)(A |)] | |
| 441 111111 | | | | | Pitiess Adapter U | lsed [Rule 338.44 (3 |)(b)] | | |
| 14) WELL TESTS: | Pollor - I-u- | | | | | tive Procedure Used | | 1] | |
| Type test: Pump | Bailer Detted |] | | | TE STORES | | | - | |
| Yield: gpm with | ft. drawdown after | hrs. | 11 |) WAT | TER LEVEL: | | | | ٠ |
| | | | | | | | | _ | |
| 15) WATER QUALITY: | A manager schiller and an inches of the control of | | | | utic level | tt. below land su | | Date _ | · · · · · · · · · · · · · · · · · · · |
| Did you knowingly penetrate any constituents? | y strata which contained undesirable | | | An | esian flow | gpm. | | Date | |
| ☐ Yes ☐ No | | | 12 |) PAC | KERS: | Туре | | | Depth |
| Type of water? | Depth of strata | | | | | | | | |
| Was a chemical analysis mad | | | Ī. | | | | | | |
| TTER C. S. POLITICAL CLICKY 918 11RX | | | - | | | | | | |
| I hereby certify that this well was drilled | hu ma for under my suncadalest and | that each and | all of t | ne stet | ements herein en | e true to the best of m | y knowledae | and belief. | <u> </u> |
| I hereby certify that this well was drilled understand that failure to complete item | is 1 thru 15 will result in the log(s) bek | ng returned for | comp | letion a | nd resubmittel. | . = = ; | | | ** |
| | Texas/Bureau of Economic | | | | | NO | 3187-M | | |
| WILLIAM SHIPPIGHT VI | (Type or Print) | | | | | | | | |
| ADDRESS P.O. BOX X | University Station | | Aus | | | | kas | 7870 | 11 |
| | (Street or RFD) | | (City) |) | | , (t | State) | (Zip) | |
| (Signed) | · · · · · · · · · · · · · · · · · · · | James Doss | (Sign | red) | | | | | ordan Forma |
| | (Licensed Well Driller) | | ٠ | | | (Regis | tered Driller T | rainee) | |
| | Please attach electric log, che | mical analysis | , and | other p | pertinent informa | rtion, if available. | - 1 · . | | 5 - S |

WATER MONITOR SCHEMATIC CAMP SWIFT #1 DRILL DATE: 11/1/95 NATIONAL GUARD PROJECT



| ATTENTION OWNER: Confidentiality Privilege Notice on Reverse Side | | | State of WELL | | | | | | | P.O. Bo | 78711-308 | • |
|---|--|---|--|--|--|--|--|---|---|---|---------------------------------------|-------------------|
| | | | Camp | Swift | #2 | | | | · ···· | | | |
| 1) OWNER Texas Nation | nal Guard | | ADDRESS | 3 | F | P.O. Bo | x 521 | В | Austi | in | Tx | 78763 |
| | (Name) | | | | | (Street | or RFD) | | (City |) | (State) | (Zip) |
| 2) ADDRESS OF WELL: | Comp Civil | # D+ 0 Bo | 1E1 P | astro | 'n | | Texas | 704 | 602-973 | 7 GRII | 59 | -54-3 |
| County Bastrop | (Street, RFE | ift Rt. 2, Bo | X 131- C | (City) | ٣ | | (State) | | (Zip) | <u>_</u> | · | |
| T | (0.004 /# 2 | 0. 02.01) | | (5.97 | | | ····· | | | | 5) | |
| 3) TYPE OF WORK (Check): | 4) PROPOS | SED USE (Ch | • — | | | Environr | | | □ Dome | | | |
| ⊠ New Well □ Deepening | ☐ Indus | | igation 🗆 Injection | | | | _ | -watering | ☐ Testv | Y O 11 | | |
| ☐ Reconditioning ☐ Plugging | If Public | Supply well, w | vere plans submitt | ed to th | o TNR | CC? | . □ Yes | □ No | | 1 1 | 30° 14' | 32" |
| 6) WELL LOG: | DIA | METER OF H | OLE | 7) | DRILI | ING ME | THOD (CI | heck): | □ Drive | ∍n | 97° 17 | 9" |
| Date Drilling: | Dis. (in.) | From (ft.) | To (ft.) | - | _ | r Rotary | | ud Rotary | . — | | 1 | |
| Started 1/3 19 96 Completed 1/3 19 96 | 7 7/8 | Surface | 50.95 | - | □ Al | r Hamme | r 🔲 Augered | Cable Too | Jett | ed | | Ň |
| | | | 1 | 1 | M C | | | | | | | . IN |
| From (ft.) To (ft.) | Description and | color of form | ation material | 8) | Borel | noie Com | pletion (| Check): | □ Op | en Hole | ⊠ Straigh | nt Wall |
| 0.0 13.5 | Light bro | own sand | | 7 | ט 🗀 | nderream | ed [| ☐ Gravel | Packed | □ Other _ | | |
| 13.5 23.5 | | | nd grey clay | 1 | If Gran | vel Packe | d give int | erval f | rom | ft. | to | |
| 23.5 28.5 | | wn clay w | | CAS | | | | | CREEN DA | | | |
| 28.5 48.5 | | | sand & clay | | New | Stee | , Plastic, | etc. | | | ng (ft.) | Gage |
| 48.5 50.75 | | d dark bro | | Die (in.) | or Used | Pert. Scre | ., Slotted, en Mig., i | etc. I commerc | lek | From | То | Casting Screen |
| 50.75 50.95 | Grey roo | | WII CIQY | 2" | N | | | iule 40 | | 2.5 Above Surface | 40.9 | |
| 50.75 50.95 | Grey ICC | <u> </u> | | 2" | N | | | | | | 50.9' | .010 |
| | | · | • | 2 | 14 | PVC | Sched | <u>iule 40</u> | - 10 | 40.9 | 30.9 | .010 |
| | | | | | | | | | | | - | |
| | | | | 1 1 | | 1 | | | | 1 . | 100 | |
| | | | | 9) | | ENTING D | 4" Above Burlece | [Rule 33 ft. to | <u>0</u> n. | | s Used | |
| (Use reven | se side if necessa | uy) | | 9) | Metho Ceme Distar | nted from od used inted by nce to ser | Hand Po | ft. to 1.1 ft. to oured w m field line | 0 ft. ft. | No. of Sack | | |
| (Use revers | se side il necesss | יעין) | | | Metho Ceme Distar Metho | nted from od used inted by nice to seri | Hand Po | ft. to 1.0 ft. to oured w field line above dis | 0_n. | No. of Sack | s Used | |
| 13) TYPE PUMP: | | uy) | | | Metho Ceme Distar Metho | nted from od used inted by nce to ser | Hand Po | ft. to 1.0 ft. to oured w field line above dis | 0 ft. ft. | No. of Sack | s Used | |
| 13) TYPE PUMP: | | | | | Metho Ceme Distar Metho | od used onted by nice to sepond of verification of the control of | Hand Portic System ication of | ft. to 1.0 ft. to | tt. tt. s or other or | No. of Sack | contamination | |
| 13) TYPE PUMP: | ubmersible | | t. | | Metho Ceme Distar Metho | od used onted by noe to sepond of verifications. | Hand Por Drill Crestic System ication of OMPLETI | ft. to 1.0 ft. to coursed w m field line above dis iON Stab Insta | tt. tt. s or other or tance N/A | No. of Sack oncentrated A | contamination | |
| 13) TYPE PUMP: ☐ Turbine ☐ Jet ☐ S | ubmersible | | tt. | | Metho Ceme Distar Metho | od used onted by nice to sepad of verification Specified Specified | Hand Po Drill Cre Dic systemication of OMPLETI Surface | ft. to 1.0 ft. to | tt. tt. s or other of tance N/A | No. of Sack oncentrated A 338.44 (2) (A | contamination | |
| 13) TYPE PUMP: ☐ Turbine ☐ Jet ☐ S | ubmersible | | t. | | Metho Ceme Distar Metho | od used onted by nice to sepad of verification Specified Specified | Hand Po Drill Cre Dic systemication of OMPLETI Surface | ft. to 1.0 ft. to | tt. tt. s or other or tance N/A | No. of Sack oncentrated A 338.44 (2) (A | contamination | |
| 13) TYPE PUMP: ☐ Turbine ☐ Jet ☐ S ☐ Other Depth to pump bowls, cylinder, | ubmersible | Cylinder | t. | | Methodo Cerme Distar Methodo SUF | od used once to sepond of verification of the control of the contr | Hand Portice System ication of OMPLETI | ft. to 1.1 ft. to bured w m field line above dis ION Slab Instaled [Rule | tt. tt. tt. N/A lied [Rule 3 338.44 (3)(| No. of Sack oncentrated A 338.44 (2) (A | contamination | |
| 13) TYPE PUMP: Turbine Jet S Other Depth to pump bowls, cylinder, | ubmersible it is to be a second or | Cylinder | tt. | 10 | Metho Ceme Distar Metho | od used once to sepond of verification of the control of the contr | Hand Por Drill Cree Drill Cree Station of OMPLETI Surface Steel State dapter Us di Alternati | ft. to 1.1 ft. to bured w m field line above dis ION Slab Instaled [Rule | tt. tt. tt. N/A lied [Rule 3 338.44 (3)(| No. of Sack oncentrated 338.44 (2) (A 338.44 (3)(A) | contamination | |
| 13) TYPE PUMP: Turbine | ubmersible , jet, etc., Baller Je | Cylinder | | 10 | Methot Ceme Distar Methot Surface Surf | od used onted by noe to sepond of verification of the sepond of the sepo | Hand Por Drill Cree Drill Cree Station of OMPLETI Surface Steel State dapter Us di Alternati | ft. to 1.0 ft. to 500000000000000000000000000000000000 | tt. tt. s or other or tance N/A lied [Rule 3 lied [Rule 3 338.44 (3)() | No. of Sack oncentrated 338.44 (2) (A 338.44 (3)(A) b)] [Rule 338.71 | contamination | |
| 13) TYPE PUMP: Turbine | ubmersible , jet, etc., Baller ft. drawdo | Cylinder | hrs. | 10 | Methological Metho | od used onted by noe to sepond of verification of the sepond of the sepo | Hand Por Drill Cree Drill Cree State State State dapter Us di Alternati | ft. to 1.0 ft. to 500000000000000000000000000000000000 | tt. tt. s or other or tance N/A lied [Rule 3 338.44 (3)() lure Used | No. of Sack oncentrated 338.44 (2) (A 338.44 (3)(A) b)] [Rule 338.71 | contamination | |
| 13) TYPE PUMP: Turbine | ubmersible , jet, etc., Baller ft. drawdo | Cylinder | hrs. | 10 | Methot Cerner Distar Methot Sur | onted from od used onted by noe to sep od of verified Specified Specified Pitiess An Approved TER LEVI | Hand Por Drill Cree Drill Cree State State State dapter Us di Alternati | ft. to 1.0 ft. to 500000000000000000000000000000000000 | tt. tt. s or other or tance N/A lied [Rule 3 338.44 (3)(lure Used | No. of Sack oncentrated 338.44 (2) (A 338.44 (3)(A) b)] [Rule 338.71 | contamination Date | on <u>N/A</u> |
| 13) TYPE PUMP: Turbine | ubmersible , jet, etc., Baller ft. drawdo | Cylinder | hrs. | 10 | Methot Cerner Distar Methot Sur | od used onted by noe to sepond of verification of the sepond of the sepo | Hand Pontice System ication of OMPLETI Surface Steel Skedapter Us di Alternati | ft. to 1.0 ft. to 500000000000000000000000000000000000 | tt. tt. s or other or tance N/A lied [Rule 3 338.44 (3)() lure Used | No. of Sack oncentrated 338.44 (2) (A 338.44 (3)(A) b)] [Rule 338.71 | contamination Date | |
| 13) TYPE PUMP: Turbine | ubmersible , jet, etc., Baller ft. drawdo | Cylinder etted wn after | hrs. | 10 | Methot Cerner Distar Methot Sur | onted from od used onted by noe to sep od of verified Specified Specified Pitiess An Approved TER LEVI | Hand Pontice System ication of OMPLETI Surface Steel Skedapter Us di Alternati | ft. to 1.0 ft. to 500000000000000000000000000000000000 | tt. tt. s or other or tance N/A lied [Rule 3 338.44 (3)(lure Used | No. of Sack oncentrated 338.44 (2) (A 338.44 (3)(A) b)] [Rule 338.71 | contamination Date | on <u>N/A</u> |
| 13) TYPE PUMP: Turbine | ubmersible , jet, etc., Baller Je ft. drawdo strata which cont | Cylinder Sted wn after mined undesira | hrs. | 10 | Methot Cerner Distar Methot Sur | onted from od used onted by noe to sep od of verified Specified Specified Pitiess An Approved TER LEVI | Hand Pontice System ication of OMPLETI Surface Steel Skedapter Us di Alternati | ft. to 1.0 ft. to 500000000000000000000000000000000000 | tt. tt. s or other or tance N/A lied [Rule 3 338.44 (3)(lure Used | No. of Sack oncentrated 338.44 (2) (A 338.44 (3)(A) b)] [Rule 338.71 | contamination Date | on <u>N/A</u> |
| 13) TYPE PUMP: Turbine | ubmersible | cylinder Sted wn after mined undesira ata | hrs. | 110 | Methodo Cermer Distar Methodo SuF | od used inted by ince to sepond of verification of the sepond of verification of the sepond of the separate sepond of the separate separate sepond of the separate | Hand Pontic System ication of OMPLETI Surface is Alternatified. | ft. to 1.1 ft. to bured w m field line above dis lON Slab Instal seve Instal ed [Rule ive Proced | tt. tt. tt. s or other or tance N/A lied [Rule 3 338.44 (3)(ii liure Used bw land surf gpm. Type | No. of Sack oncentrated A 338.44 (2) (A 338.44 (3)(A) b)] [Rule 338.71 | contamination | on <u>N/A</u> |
| 13) TYPE PUMP: Turbine | ubmersible | cylinder cited wn after mined undesira ata ny supervision) | hrs. | 10 11 12 12 13 14 16 16 16 16 16 16 16 16 16 16 16 16 16 | Methor Cerner Distar Methor Sur Sur Sur Sur Sur Sur Sur Sur Sur Su | od used onted by noe to sepond of verification of the sepond of the sepo | Hand Pontic System ication of OMPLETI Surface is Steel Sidapter Us di Alternati | ft. to 1.1 ft. to bured w m field line above dis lON Slab Instal seve Instal ed [Rule ive Proced | tt. tt. tt. s or other or tance N/A lied [Rule 3 338.44 (3)(ii liure Used bw land surf gpm. Type | No. of Sack oncentrated A 338.44 (2) (A 338.44 (3)(A) b)] [Rule 338.71 | contamination | on <u>N/A</u> |
| 13) TYPE PUMP: Turbine | ubmersible | etted win after ata No y supervision) uit in the log(s) | hrs. shiple and that each and being returned for | 110 111 112 112 112 113 113 113 113 113 113 | Methot Cerner Distart Methot SUF | onted from ad used inted by noe to sep ad of verification Specified Specified Pitiess An Approved TER LEVI title level estan flow CKERS: | Hand Portic System ication of OMPLETI Surface I Steel Skedapter Us Alternati EL: | ft. to 1.1 ft. to bured w m field line above dis lon Slab Instal seve Instal ed [Rule ive Proced ft. bek | tt. ft. ft. s or other or tance N/A lied [Rule 3 338.44 (3)(i) liure Used pw land surf gpm. Type | No. of Sack oncentrated A 338.44 (2) (A 338.44 (3)(A) b)] [Rule 338.71 | contamination | on <u>N/A</u> |
| 13) TYPE PUMP: Turbine | bubmersible | etted win after | hrs. shiple and that each and being returned for | 110 111 112 112 112 113 113 113 113 113 113 | Methor Cerne Distar Methor SUF | onted from ad used inted by noe to sep ad of verification Specified Specified Pitiess An Approved TER LEVI title level estan flow CKERS: | Hand Portic System ication of OMPLETI Surface I Steel Skedapter Us Alternati EL: | ft. to 1.1 ft. to bured w m field line above dis loN Slab Instal seve Instal led [Rule ive Proced ft. bek | tt. ft. ft. s or other or tance N/A lied [Rule 3 338.44 (3)(i) liure Used pw land surf gpm. Type | No. of Sack concentrated A 338.44 (2) (A 338.44 (3)(A) b)] [Rule 338.71 | contamination | Depth |
| 13) TYPE PUMP: Turbine | bubmersible | etted win after | hrs. shiple and that each and being returned for | 110 12 12 diali of tor comple | Methor Ceme Distar Methor Sur Distar Methor Distar Methor Distar | onted from ad used inted by noe to sep ad of verification Specified Specified Pitiess An Approved TER LEVI title level estan flow CKERS: | Hand Portic System ication of OMPLETI Surface I Steel Skedapter Us Alternati EL: | ft. to 1.1 ft. to bured w m field line above dis loN Slab Instal seve Instal led [Rule ive Proced ft. bek | tt. tt. s or other or tance N/A lied [Rule 3 lied [Rule 3 338.44 (3)() lure Used [bw land surf gpm. Type | No. of Sack concentrated A 338.44 (2) (A 338.44 (3)(A) b)] [Rule 338.71 | contamination Date Date Date Date | on <u>N/A</u> |

WATER MONITOR SCHEMATIC CAMP SWIFT #2 DRILL DATE: 1/3/96 NATIONAL GUARD PROJECT



Appendix 3

Water-Level and Water-Quality Data from Powell Bend Mine

Appendix 3. Water-level and water-quality data from Powell Bend Mine.

Well TU-58

Depth: 115 ft

| Date | Water level (ft amsl*) | C1 (mg L ⁻¹) | Fe (mg L ⁻¹) | Mn (mg L ⁻¹) | TDS (mg L ⁻¹) | SO ₄ (mg L ⁻¹) | pН |
|---------|------------------------|--------------------------|--------------------------|-----------------------------|---------------------------|---------------------------------------|------|
| 1987.00 | 350.9 | 43 | 3.22 | 0.67 | 636 | 144 | 6.7 |
| 1987.75 | 350.5 | 48 | 3.24 | 0.65 | 710 | 204 | 6.5 |
| 1988.25 | 351 | 47 | 2.5 | 0.62 | 608 | 136 | 6.9 |
| 1988.50 | | 51 | 2.42 | 1.14 | 632 | 75 | 6.88 |
| 1988.75 | 350.7 | 43 | 2.29 | 0.53 | 626 | 120 | 7 |
| 1989.00 | 350.4 | 18 | 2.2 | 0.56 | 578 | 100 | 6.8 |
| 1989.25 | 350.5 | 40 | 3.12 | 0.73 | 573 | 128 | 7 |
| 1989.50 | 349.9 | 42 | 2.35 | 0.56 | 601 | 139 | 6.7 |
| 1989.75 | 349.6 | 41 | 2.27 | 0.57 | 572 | 133 | 6.6 |
| 1990.00 | 349.1 | 40 | 2.72 | 0.58 | 528 | 125 | 7.3 |
| 1990.25 | 349 | 41 | 2.61 | 0.58 | 636 | 127 | 6.7 |
| 1990.75 | 349.1 | 41 | 2.6 | 0.65 | 617 | 132 | 6.8 |
| 1991.00 | 350 | 40 | 2.82 | 0.61 | 597 | 115 | 6.9 |
| 1991.25 | 350 | 42 | 2.51 | 0.55 | 616 | 121 | 6.9 |
| 1991.50 | 350 | 47 | 2.17 | 0.36 | 560 | 130 | 6.9 |
| 1991.75 | 350 | 45 | 2.57 | 0.63 | 574 | 145 | 6.8 |
| 1992.00 | 351 | 43 | 3.22 | 0.54 | 526 | 125 | 6.8 |
| 1992.25 | 352.9 | 56 | 2.66 | < 0.01 | 605 | 163 | 6.92 |
| 1992.50 | 353.6 | 57 | 2.66 | 0.55 | 597 | 130 | 7.12 |
| 1992.75 | 353 | 74 | 2.21 | 0.29 | 301 | 41 | 7.3 |
| 1993.00 | 352 | 57 | 5.92 | 0.51 | 702 | 113 | 6.78 |
| 1993.25 | 355 | 57 | 5.66 | 0.15 | 685 | 204 | 6.65 |
| 1993.50 | 353 | 145 | 7.54 | 1.1 | 1606 | 694 | 6.85 |
| 1993.75 | 351 | 211 | 7.52 | 1.43 | 1811 | 216 | 6.76 |
| 1994.00 | 353 | 212 | 7.85 | , - | 2179 | 700 | 6.48 |
| 1994.25 | 352.3 | 224 | 11.62 | 2.47 | 2692 | 1309 | 6.49 |
| 1994.50 | 351 | 167 | 10.47 | 1.6 | 2122 | 1050 | 6.5 |
| 1994.75 | 352 | 278 | 8.54 | 1.63 | - | 986 | 6.13 |
| 1995.50 | 354 | _ | - | - | - | · .* | - |

Well TU-151

Depth: 80 ft

| Date | Water level (ft amsl*) | Cl (mg L ⁻¹) | Fe (mg L ⁻¹) | Mn (mg L ⁻¹) | TDS (mg L ⁻¹) | SO ₄ (mg L ⁻¹) | pН |
|---------|------------------------|--------------------------|--------------------------|--------------------------|---------------------------|---------------------------------------|------|
| 1987.00 | 406.8 | 44 | 3.96 | 0.75 | 1980 | 143 | 6.8 |
| 1987.75 | 406.3 | 320 | 2.87 | 0.77 | 2000 | 713 | 6.2 |
| 1988.25 | 407.4 | 301 | 4.01 | 0.7 | 1948 | 627 | 6.7 |
| 1988.50 | - | 343 | 3.5 | 0.83 | 2018 | 724 | 6.68 |
| 1988.75 | 405.3 | 315 | 3.6 | 0.73 | 2020 | 725 | 6.8 |
| 1989.00 | 404.1 | 49 | 3.89 | 0.72 | 2208 | 540 | 6.6 |
| 1989.25 | 404.1 | 290 | 4.45 | 0.91 | 2035 | 660 | 6.7 |
| 1989.50 | 403.3 | 326 | 3.91 | 0.71 | 1932 | 728 | 6.6 |
| 1989.75 | 402.4 | 301 | 2.13 | 0.64 | 1927 | 734 | 6.6 |
| 1990.00 | 403.4 | 323 | 3.45 | 0.66 | 1980 | 710 | 7.1 |
| 1990.25 | 403.4 | 325 | 3.66 | 0.71 | 2214 | 682 | 6.6 |
| 1990.75 | 403.4 | 333 | 3.63 | 0.78 | 2136 | 675 | 6.6 |
| 1991.00 | 401.6 | 332 | 3.98 | 0.78 | 1920 | 710 | 6.7 |
| 1991.25 | 401.6 | 334 | 4.04 | 0.74 | 2264 | 802 | 6.7 |
| 1991.50 | 402.1 | 309 | 0.15 | 0.52 | 2221 | 748 | 6.8 |
| 1991.75 | 401.8 | 319 | 4.04 | 0.71 | 1936 | 772 | 6.7 |
| 1992.00 | 402.8 | 346 | 4.06 | 0.77 | 2142 | 812 | 6.7 |
| 1992.25 | 406 | 301 | < 0.01 | < 0.01 | 2915 | 832 | 6.79 |
| 1992.50 | 409 | 367 | 3.79 | 0.75 | 2362 | 841 | 6.74 |
| 1992.75 | 399 | 56 | 3.89 | 0.5 | 667 | 80 | 6.9 |
| 1993.00 | 398 | 42 | 23.88 | 0.64 | 707 | 103 | 6.79 |
| 1993.25 | 413 | 70 | 1.3 | 0.08 | 514 | 74 | 7.17 |
| 1993.50 | 412 | 315 | 7.92 | 0.81 | 1962 | 660 | 6.85 |
| 1993.75 | 410 | 310 | 7.79 | 0.76 | 2029 | 702 | 6.73 |
| 1994.00 | 409 | 303 | 2.08 | <u>.</u> - | 1934 | 584 | 6.62 |
| 1994.25 | 406.6 | 241 | 4.2 | 0.81 | 1960 | 730 | 8.24 |
| 1994.50 | 406 | 322 | 4.65 | 0.64 | 2504 | 650 | 6.81 |
| 1994.75 | 420 | 332 | 2.53 | 0.62 | - | 842 | 6.68 |
| 1995.50 | 417.1 | - | · - | - | - | - | - |

Well TU-193

Depth: 75 ft

| | Water level | Cl 1 | Fe | Mn | TDS | SO ₄ | |
|---------|-------------|----------------------|----------------------|-----------------------|-----------------------|-----------------------|--------|
| Date | (ft amsl*) | (mg L^{-1}) | (mg L^{-1}) | (mg L ⁻¹) | (mg L ⁻¹) | (mg L ⁻¹) | pН |
| 1987.00 | 402.3 | 828 | 2.18 | 0.37 | 2340 | 95 | 7 |
| 1987.75 | 401.6 | 796 | 2.11 | 0.34 | 1958 | 80 | 6.6 |
| 1988.25 | 402.2 | 683 | 2.03 | 0.4 | 2360 | 66 | 7.1 |
| 1988.50 | - | 915 | 0.28 | 0.23 | 2614 | 97 | 7.06 |
| 1988.75 | 402.4 | 840 | 2 | 0.27 | 2142 | 65 | 7.1 |
| 1989.00 | 402.2 | 860 | 2.81 | 0.42 | 2610 | 28 | 6.8 |
| 1989.25 | 402.1 | 850 | 2.38 | 0.39 | 2335 | 74 | 7.1 |
| 1989.50 | 402.9 | 859 | 2.11 | 0.36 | 1977 | 96 | 6.9 |
| 1989.75 | 402.4 | 866 | 2.39 | 0.34 | 2246 | 90 | 7 |
| 1990.00 | 402.2 | 846 | 3.41 | 0.33 | 2345 | . 87 | 7.5 |
| 1990.25 | 402 | 884 | 2.17 | 0.4 | 2315 | 44 | 7.1 |
| 1990.75 | 402 | 831 | 1.94 | 0.37 | 2256 | . 73 | 6.9 |
| 1991.00 | 401.6 | 332 | 3.98 | 0.78 | 1920 | 710 | 6.7 |
| 1991.25 | 402.2 | 118 | 0.07 | 0.01 | 644 | 89 | 7.8 |
| 1991.50 | 402.2 | 893 | 1.82 | 0.12 | 2104 | 88 | 7 |
| 1991.75 | 402.4 | 839 | 2.19 | 0.31 | 2238 | 81 | 7 7 |
| 1992.00 | 402.2 | 856 | 2.39 | 0.28 | 2183 | 86 | |
| 1992.25 | 402.42 | 475 | 2.34 | < 0.01 | 2723 | 91 | 6.93 |
| 1992.50 | 403.6 | 1024 | 2.79 | 0.33 | 2286 | 28 | 6.99 |
| 1992.75 | 404 | 839 | 2.69 | 0.36 | 2316 | . 5 | 7.3 |
| 1993.00 | 401 | 888 | 2.4 | 0.32 | 218* | 27 | 7 |
| 1993.25 | 409.22 | 709 | 2.75 | 0.34 | 2830 | 70 | 6.94 |
| 1993.50 | 407 | 909 | 2.13 | 0.34 | 2503 | 428 | 7 |
| 1993.75 | 405 | 911 | 4.48 | 0.37 | 2851 | 97 | 7.06 |
| 1994.00 | 403 | 847 | 2.41 | . - | 2132 | 74 | 6.92 |
| 1994.25 | 403.2 | 84 | 3.14 | 0.33 | 2556 | 67 | 7.19 |
| 1994.50 | 403 | 864 | 2.19 | 0.3 | 3356 | 50 | 7.13 |
| 1994.75 | 407 | 848 | 2.11 | 0.29 | - ' | 33 | 7 |
| 1995.50 | 411.22 | • | <u>-</u> | - | | | - |

Well TU-194

Depth: 145 ft

| | Water level | C1 | Fe | Mn | TDS | SO ₄ | |
|---------|-------------|---------------|----------------------|-----------------------|----------------------|----------------------|------|
| Date | (ft amsl*) | $(mg L^{-1})$ | (mg L^{-1}) | (mg L ⁻¹) | (mg L^{-1}) | (mg L^{-1}) | pН |
| 1987.00 | 348.8 | 62 | 10.91 | 0.57 | 964 | 74 | 7.2 |
| 1987.75 | 347.8 | 62 | 14.2 | 0.64 | 788 | 72 | 8.3 |
| 1988.25 | 348.7 | 67 | 4.7 | 0.68 | 494 | 76 | 7.2 |
| 1988.50 | - | 69 | 22.45 | 1.1 | 516 | 83 | 7.35 |
| 1988.75 | 349.1 | 61 | 19.9 | 0.51 | 372 | 74 | 7.3 |
| 1989.00 | 349.4 | 59 | 5.73 | 0.49 | 506 | 73 | 7 |
| 1989.25 | 348.8 | 56 | 5.45 | 0.64 | 586 | 68 | 7.1 |
| 1989.50 | 348.7 | 56 | 5.45 | 0.64 | 586 | 68 | 7.1 |
| 1989.75 | 348.7 | 60 | 7.04 | 0.54 | 569 | . 75 | 7.1 |
| 1990.00 | 348 | 62 | 40.37 | 1.34 | 502 | 75 | 7.6 |
| 1990.25 | 348.2 | 64 | 3.51 | 0.6 | 504 | 69 | 7.2 |
| 1990.75 | 348 | 63 | 6.5 | 0.61 | 522 | 71 | 7 |
| 1991.00 | 348.1 | 61 | 11.03 | 0.72 | 485 | 64 | 7.1 |
| 1991.25 | 348.1 | 106 | 0.02 | 0.01 | 2200 | 81 | 7 |
| 1991.50 | 347.1 | 59 | 1.27 | 0.36 | 584 | 77 | 7.2 |
| 1991.75 | 348.1 | 60 | 4.48 | 0.57 | 480 | 75 | 7 |
| 1992.00 | 348.6 | 62 | 5.41 | 0.54 | 535 | 69 | 7.3 |
| 1992.25 | 348.76 | 66 | 2.91 | 0.53 | 601 | 78 | 7.16 |
| 1992.50 | 349 | 69 | 5.33 | 0.46 | 479 | 68 | 7.25 |
| 1992.75 | 349 | 63 | 2.13 | 0.41 | 593 | 40 | 7.4 |
| 1993.00 | 349 | 60 | 10.12 | 0.59 | 483 | 62 | 7.2 |
| 1993.25 | 352.06 | - · | <u>-</u> | - | | · <u>-</u> . · | - |
| 1993.50 | 351 | 65 | 2.29 | 0.36 | 487 | 82 | 7.33 |
| 1993.75 | 356 | 78 | 5.42 | 0.44 | 489 | 79 | 7.22 |
| 1994.00 | 350 | 59 | 3.89 | _ | 502 | 155 | 7.12 |
| 1994.25 | 350.6 | 84 | 9.65 | 0.56 | 510 | 6 | 7.33 |
| 1994.50 | 350 | 64 | 7.74 | 0.5 | 744 | 50 | 7.17 |
| 1994.75 | 350 | 86 | 4.12 | 0.43 | _ ` | 118 | 7.05 |
| 1995.50 | 351.06 | | _ : | · , · · - | _ | <u>.</u> . | - |
| | | | | | | | |

Well TU-195

Depth: 115 ft

| | Water level | Cl | Fe | Mn | TDS | SO_4 | |
|---------|-------------|----------------------|---------------|-----------------------|----------------------|----------------------|------|
| Date | (ft amsl*) | (mg L^{-1}) | $(mg L^{-1})$ | (mg L ⁻¹) | (mg L^{-1}) | (mg L^{-1}) | pН |
| 1987.00 | 348.9 | 73 | 0.18 | 0.12 | 556 | 85 | 7.2 |
| 1987.75 | 348.3 | 67 | 0.38 | 0.16 | 472 | 67 | 6.9 |
| 1988.25 | 349.6 | 68 | 0.22 | 0.12 | 468 | 64 | 7.3 |
| 1988.50 | - | 78 | 0.58 | 0.2 | 534 | 75 | 7.28 |
| 1988.75 | 349.4 | 73 | 0.42 | 0.09 | 500 | 85 | 7.3 |
| 1989.00 | 348.8 | 48 | 0.45 | 0.17 | 644 | 76 | 7.2 |
| 1989.25 | 349.2 | 40 | 0.6 | 0.23 | 513 | 128 | 7.3 |
| 1989.50 | 348.6 | 74 | 0.61 | 0.2 | 519 | 90 | 7.1 |
| 1989.75 | 348.4 | 74 | 0.44 | 0.24 | 501 | 85 | 6.9 |
| 1990.00 | 348.5 | 72 | 0.6 | 0.2 | 472 | 79 | 7.7 |
| 1990.25 | 348.5 | 74 | 0.62 | 0.21 | 530 | 80 | : 7 |
| 1990.75 | 348.6 | 76 | 0.5 | 0.24 | 508 | . 75 | 7.2 |
| 1991.00 | 348.2 | 72 | 0.49 | 0.17 | 557 | 67 | 7.3 |
| 1991.25 | 348.2 | 148 | 0.56 | 0.16 | 492 | 154 | 7.3 |
| 1991.50 | 347.6 | 72 | 0.4 | 0.01 | 524 | 75 | 7.3 |
| 1991.75 | 348.4 | 73 | 0.42 | 0.13 | 487 | 88 | 7.2 |
| 1992.00 | 348.6 | 69 | 0.51 | 0.15 | 500 | 74 | 7.3 |
| 1992.25 | 349.35 | 74 | 0.63 | < 0.01 | 479 | 72 | 7.22 |
| 1992.50 | 349 | 74 | 0.84 | 0.09 | 468 | 45 | 7.33 |
| 1992.75 | 349 | 265 | 1.08 | 0.27 | 2188 | 375 | 7.3 |
| 1993.00 | 350 | 68 | 4.25 | 0.54 | 512 | 70 | 7.22 |
| 1993.25 | 353.28 | 69 | 1.78 | 0.36 | 514 | . 77 | 7.21 |
| 1993.50 | 350.5 | 75 | 0.92 | 0.2 | 503 | 82 | 7.26 |
| 1993.75 | 352 | 62 | 1.78 | 0.23 | 521 | 81 | 7.26 |
| 1994.00 | 350 | 74 | 2.73 | - | 557 | 143 | 7.12 |
| 1994.25 | 351.5 | 51 | 1.26 | < 0.01 | 518 | 42 | 7.44 |
| 1994.50 | 349 | 77 | 1.21 | 0.86 | 628 | 91 | 7.26 |
| 1994.75 | 352 | 72 | 1.53 | 1.13 | - | 96 | 7.19 |
| 1995.50 | 353.55 | - | | - | - | · | - |

Appendix 3 (cont.)

Well BPB-WW1

| | Water level | Cl | Fe | Mn | TDS | SO ₄ | |
|---------|----------------|---------------|---------------|---------------|----------------------|-----------------------|------|
| Date | (ft amsl*) | $(mg L^{-1})$ | $(mg L^{-1})$ | $(mg L^{-1})$ | (mg L^{-1}) | (mg L ⁻¹) | pН |
| 1987.00 | - · | 49 | 0.76 | 0.16 | 478 | 36 | 7.4 |
| 1987.75 | . = | 49 | 0.58 | 0.15 | 418 | 36 | 7.4 |
| 1988.25 | <u>-</u> | 52 | 1.84 | 0.25 | 396 | 37 | 7.3 |
| 1988.50 | - | 58 | 1.79 | 0.45 | 516 | 40 | 7.45 |
| 1988.75 | | 53 | 0.78 | 0.09 | 374 | 39 | 7.5 |
| 1989.00 | <u>-</u> | 22 | 0.89 | 0.16 | 478 | 21 | 7.3 |
| 1989.25 | . - | 46 | 1.25 | 0.23 | 414 | 34 | 7.4 |
| 1989.50 | - | 47 | 0.41 | 0.19 | 497 | 41 | 7.4 |
| 1989.75 | - | 49 | 0.57 | 0.17 | 488 | 38 | 7.4 |
| 1990.00 | - | 49 | 0.59 | 0.2 | 376 | 40 | 8.1 |
| 1990.25 | | 52 | 0.53 | 0.09 | 397 | 37 | 7.5 |
| 1990.75 | - | 52 | 0.48 | 0.22 | 452 | 39 | 7.4 |
| 1991.00 | · | 52 | 0.88 | 0.2 | 404 | 40 | 7.3 |
| 1991.25 | - | 120 | 0.6 | 0.14 | 426 | 89 | 7.6 |
| 1991.50 | · - | . 48 | 0.01 | 0.01 | 455 | 36 | 7.9 |
| 1991.75 | - | 52 | 0.98 | 0.17 | 458 | 42 | 7.6 |
| 1992.00 | · | 56 | 0.66 | 0.18 | 441 | 42 | 7.4 |
| 1992.25 | - | 58 | 0.7 | < 0.01 | 428 | 39 | 7.58 |
| 1992.50 | · '= | 57 | 1.8 | 0.17 | 375 | 22 | 7.44 |
| 1992.75 | · - . | 55 | 1.46 | 0.24 | 400 | 21 | 7.6 |
| 1993.00 | 272 | 52 | 1.83 | 0.25 | 382 | 33 | 7.48 |
| 1993.25 | 237.28 | 51 | 0.4 | 0.18 | 390 | 29 | 7.71 |
| 1993.50 | 231 | 55 . | 1.06 | 0.21 | 393 | 51 | 7.69 |
| 1993.75 | 361 | 49 | 0.27 | 0.04 | 373 | 33 | 8.17 |
| 1994.00 | 365 | 50 | 1.7 | - | 387 | 42 | 7.58 |
| 1994.25 | 231 | 53 | 0.04 | < 0.01 | 350 | 26 | 7.97 |
| 1994.50 | 237 | 52 | 0.05 | 0.01 | 366 | 31 | 7.75 |
| 1994.75 | 361 | 51 | 0.11 | 0.01 | - 4, | 36 | 7.77 |
| 1995.50 | 237.28 | · | - | - | · - | - | - |
| | | | | | | | |

^{*}amsl = above mean sea level

Appendix 4 Data Dictionary for GIS Coverages

GIS DATA DICTIONARY

Several layers of spatial hydrologic and hydrogeologic data were input to the Bureau of Economic Geology GIS system. Maps were digitized using a Calcomp digitizing table, under the ArcEdit module of GIS ArcInfo, on a Sparc500 Workstation. When possible, the data from the paper originals of the U.S. Geological Survey (USGS) 1:24,000-scale, 7.5-minute topographic maps were either transferred on Mylar or digitized during one session to minimize the distortions related to environmental factors. The digital data base, regardless of the original projection, will be delivered in the Universal Transverse Mercator (UTM) coordinate system, with the following parameters:

Ellipsoid: Clarke 1866

Horizontal Datum: NAD27

Units: meters

Zone 14

The digital data represent the following.

Digital Elevation Models (DEM) were acquired from MicroPath at 1:24,000 scale, where available (View, Buffalo Gap, Paris, Lake Bastrop, Elgin East, McDade, Graford East, Mineral Wells East, Mineral Wells West, and Whitt), or were created from digital elevation contours and streams using the Grid module of ArcInfo (Topogrid). The cell size for DEMs is 30 m, with a horizontal accuracy of ± 3 m and a vertical accuracy of ± 10 m. The DEMs were used to delineate watersheds of interest.

Watersheds represent polygon coverages encompassing the drainage areas. They were outlined from DEMs for Camp Swift, Camp Mabry, Camp Barkeley, and Fort Wolters or were defined from USGS topographic quads and then transferred to a digital format. Possible inaccuracy might be related to human error and imperfections of the digitizing equipment. Given the USGS-stated positional accuracy of ± 40 ft for its 7.5-minute quads, and the inadvertent positional shifts that may have been introduced during the digitizing process, it can be estimated that the positional accuracy of most features will be approximately ± 50 ft.

Floodplains are polygon coverages, digitized from USGS topographic quads, with the aforementioned accuracy estimate.

Well locations are point coverages, digitized from USGS topographic quadrangles; they include existing and recently drilled wells, with an internally assigned well name (number) as an item in the Point Attribute Table (PAT). They include wells on and around the camps.

Soil maps are generalized soil maps at 1:250,000 scale compiled by the U.S. Department of Agriculture Soil Conservation Service. They contain polygons describing groups of soil types and attached attribute tables with extensive sets of numerical values, including their

hydrologic properties, which were used to specify the percentage of the map unit occupied by soils in each hydrologic group. The digital data were obtained from the Texas Natural Resources Information System (TNRIS) ftp site.

Water levels represent water-level contours, which, owing to scarcity of control points and the inherent interpolation problems of the software, were hand drawn and then digitized from Mylar overlays.

Cultural features include roads and generalized streams at 1:24,000 scale, at various extents around the camp. They were obtained from the TNRIS ftp site and are the latest version of Texas Department of Transportation (TxDOT) urban maps. These files were originally digitized from USGS 7.5-minute quadrangles. Updates are made periodically using TxDOT highway construction plans, aerial photographs, official city maps, and field inventory. These files contain most of the features found on 7.5-minute quads, except for items such as contour lines, fence lines, jeep trails, electrical transmission lines, oil and gas pipelines, and control data monuments.

The county map files are based on the following map projection system:

TEXAS STATEWIDE MAPPING SYSTEM (NAD27)

Projection: Lambert Conformal Conic

Ellipsoid: Clarke 1866

Datum: North American 1927

Longitude of Origin: 100 degrees west (-100)

Latitude of Origin: 31 degrees 10 minutes north

Standard Parallel #1: 27 degrees 25 minutes north latitude Standard Parallel #2: 34 degrees 55 minutes north latitude

False Easting: 3,000,000 ft False Northing: 3,000,000 ft

Unit of Measure: feet (international)

Positional Accuracy: These digital maps were created primarily for the purpose of producing county/urban published maps. Certain features, particularly railroads and streams, have been displaced in congested areas so as to insure map readability at county map scales.

Miscalculation of false northing and easting required reprojection of the DGN digital files, at the correct values (914,400 ft), in order to obtain the perfect overlay with several preexisting county and quadrangle files.

CAMP SWIFT Base maps: the USGS 7.5' topographic quadrangles, McDade, Elgin East, and Lake Bastrop, are in the State Plane coordinate system, Central Zone (5351), datum NAD27, units in feet.

| Coverage | Coverage | Initial | Final | | | |
|--------------|----------|-----------------------------|------------|--|-----------------------|---|
| name | type | projection | projection | Source | Accuracy | Description |
| Offcamprdutm | Arc | Texas State Plane | UTM | TXDOT digital county files | ±50 ft | Highways and off-camp well locations |
| Arcamprdutm | Arc | Texas State Plane | MLO | TXDOT digital county files | ±50 ft | Highways near the camp |
| Boundutm | Polygon | State Plane Central Zone | MLO | Texas Parks and Wildlife digital files | unknown | Camp boundary |
| Streamsutm | Arc | MTD | ML | Delineated from DEM | ±40 ft | Streams and rivers in the contributing watersheds delineated from watershed analysis; threshold = 5,000 |
| Wshedutm | Polygon | UTM | UTM | Digitized from USGS 7.5' topographic quads | ±40 ft | Watersheds corresponding to stream segments |
| Fplainutm | Polygon | State Plane Central Zone | UTM | Digitized from USGS 7.5' topographic quads | ±40 ft RMS = 0.005 | Floodplains |
| Fpstreamutm | Arc | State Plane Central Zone | MTM | Digitized from USGS 7.5' topographic quads | ±40 ft RMS = 0.004 | Stream orders and cross sections used for the HEC-RAS model |
| Soilsutm | Polygon | Texas State Plane | MLN | STATSGO digital database | unknown | 1:2,500,000-scale distribution of soils in the watersheds |
| Sfswellsutm | Point | State Plane Central Zone | UTM . | Digitized from USGS 7.5' topographic quads | ±40 ft RMS = 0.004 | Location of off-camp wells |
| Sfcwellsutm | Point | State Plane Central Zone | UTM | Digitized from USGS 7.5' topographic quads | ±40 ft RMS = 0.002 | Location of on-camp wells |
| Wievels | Arc | State Plane Central Zone | MTU | Digitized from USGS 7.5' topographic quads | ±40 ft RMS = 0.005 | Digitized water-level contour maps |